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## Dear Robert

## 301-303 BUCKLAND ROAD- CLAUSE 23 RESPONSE (TRAFFIC ENGINEERS DISCUSSION)

Following production of Clause 23 responses, we have met with Council consultant Traffic Engineer (Mr Wes Edwards form Arrive). Following this meeting, Mr Edward has provided comments on the remaining items. The commentary below relates to the items noted as requiring additional information.

## 1 ITEM T1: INTENSIVE SCENARIO

You've noted one of the roundabouts may have poor performance and suggested an additional lane could sort that out. It would be good to have a concept design demonstrating that the additional lane is both practicable and effective.

## Comment:

As noted in the previous response, with the $100 \%$ LFR both roundabouts experience pressure on a Saturday peak with the new PPC / PU-NS-2 Road roundabout just reaching typical capacity levels however the Kitchener Road / Manukau Road roundabout exceeding capacity. In this regard:

- As previously noted, we consider the $100 \%$ LFR scenario "highly unlikely". This is reinforced by the economic expert who has stated "...Within the context of these limitations, a potential outcome for the site would be one third large format retail (near the road), one third industrial (further back from the road) and one third other uses".
- The $100 \%$ LFR scenario has not allowed for multi-purpose / linked trips (those that may also visit other stores on the same Plan Change or other plan Change) or pass-by traffic (ie those vehicles already on the road network that deviate into the site)
- Any future activity would be also subject to E27 E27.6.1. "Trip generation" rule of the Unitary Plan. This rule if triggered (which is generally over 100 movements or in the case of retail anything over 1667 sqm ) requires a further assessment of transport, traffic or trip-generation effects for the activity. If the site is predominantly LFR this rule will be triggered. At this time (Resource Consent) the exact land-use will be known and thus a re-assessment will need to be undertaken.

Regardless of the above Appendix A shows the potential for increasing the number of lanes at the two roundabouts. Of note there is not the space for a full two-lane roundabout at Kitchener Road / Manukau Road roundabout.

Appendix A also shows an alternative of a signalised intersection at the Kitchener Road / Manukau Road intersection. A signalised intersection at this location (as shown) would provide considerable
additional capacity than a single-lane roundabout. This is evidence in the results of this signalised intersection using the $100 \%$ LFR scenario.

## ITEM T6: 2036 SCENARIO

Future/ Growth. As discussed, the historical AT traffic counts show growth of around 1.5\% pa daily (average) with peak hours at between $1.2 \%$ and $3.2 \%$. I can't see why growth over the next 10 years or so would be less than that, so we need to either assume similar growth or have some robust data to indicate why it would be anything different.

## Comment:

For the critical Saturday peak period the growth over the last 6-7 years is equivalent to $1.5 \%$. Over 10 years in the future this would add $15 \%$ to the existing traffic. We do note that the development of the site itself will contribute to this background growth. The $100 \%$ LFR scenario has been tested with this growth and is contained in Table 1 and 2 below. An alternative signalised intersection at Kitchener Road / Manukau Road has also been modelling in Table 3.

Table 1: Proposed performance of the Manukau Road/ Kitchener Road/ Buckland Road roundabout Sat 100\% LFR 15\% growth

| Leg | Movement | Degree of Saturation (v/c) | Average <br> Delay (s) | LOS | $\begin{aligned} & 95^{\text {th }} \% \text { ile } \\ & \text { Queue (m) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Buckland Road (South) | LT | 1.149 | 156 | F | 855 |
|  | TH | 1.149 | 156 | F | 855 |
|  | RT | 1.149 | 162 | F | 855 |
| Gate 2 (main site access) (east) | LT | 0.873 | 64 | E | 107 |
|  | TH | 0.873 | 64 | E | 107 |
|  | RT | 0.873 | 70 | E | 107 |
| Manukau Road (north) | LT | 1.136 | 134 | F | 1114 |
|  | TH | 1.136 | 134 | F | 1114 |
|  | RT | 1.136 | 140 | F | 1114 |
| Kitchener Rd (west) | LT | 1.312 | 329 | F | 685 |
|  | TH | 1.312 | 329 | F | 685 |
|  | RT | 1.312 | 329 | F | 685 |

Table 2: Proposed performance of the PU-NS-2 Road / Buckland Road intersection Sat roundabout Sat 100\% LFR 15\% growth

| Leg | Movement | Degree of Saturation (v/c) | Average Delay (s) | LOS | 95 ${ }^{\text {th }} \%$ ile Queue (m) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Buckland Road (South) | LT | 1.127 | 146 | F | 586 |
|  | TH | 1.127 | 146 | F | 586 |
|  | RT | 1.127 | 151 | F | 586 |
| Racecourse Gate | LT | 0.138 | 23 | c | 8 |
|  | TH | 0.138 | 23 | C | 8 |
|  | RT | 0.138 | 28 | C | 8 |
| Buckland Road (north) | LT | 0.980 | 32 | C | 311 |
|  | TH | 0.980 | 32 | C | 311 |
|  | RT | 0.980 | 37 | D | 311 |


| Site access (PU-NS-2 | LT | 1.031 | 72 | F | 378 |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Road) (west) | TH | 1.031 | 72 | F | 378 |
|  | RT | 1.031 | 77 | $F$ | 378 |

Table 3: Proposed performance of the Manukau Road/ Kitchener Road/ Buckland Road signals Sat 100\% LFR 15\% growth

| Leg | Movement | Degree of Saturation (v/c) | Average Delay (s) | LOS | $\begin{aligned} & 95^{\text {th }} \% \text { ile } \\ & \text { Queue (m) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Buckland Road (South) | LT | 0.077 | 19 | B | 18 |
|  | TH | 0.808 | 49 | D | 256 |
|  | RT | 0.209 | 70 | E | 23 |
| Gate 2 (main site access) (east) | LT | 0.052 | 142 | D | 11 |
|  | TH | 0.979 | 105 | F | 183 |
|  | RT | 0.979 | 110 | F | 183 |
| Manukau Road (north) | LT | 0.490 | 18 | B | 64 |
|  | TH | 0.957 | 82 | F | 405 |
|  | RT | 0.973 | 109 | F | 150 |
| Kitchener Rd (west) | LT | 0.710 | 29 | C | 92 |
|  | TH | 0.961 | 98 | F | 107 |
|  | RT | 0.961 | 104 | F | 107 |

The results shows that the intersections will both be at / slightly over capacity on a Saturday peak period with these assumptions (again considered highly unlikely). The results do however show that the signalised option can cater for the traffic expected. As a result, there are upgrades possible within the road reserve and the site to appropriate serve the Plan Change even if essentially all worst-case scenarios occur (all development is LFR, growth occurs all in addition to the proposal, and no allowance is made for pass-by / multi-purpose trips). Note as per Item T 8 below, this alanysis also already includes base survey traffic of Pukekohe Park's busiest horse racing event (Counties Cup).

The exact upgrade should be determined a Resource Consent time when the exact use of the site is known.

## 2 ITEM T8: PUKEKOHE PARK

Pukekohe Park Events. Pukekohe Park is a "nationally important venue" and we need to make sure it can continue to operate as such with development in place (and also know the proposed development site could operate well when events are on). This issue is made more significant as GBZ is proposed rather than LIZ as assumed previously, and GBZ activities are more likely to overlap with events (or even be busiest when events are on). As events for up to 5000 people are permitted without any TMP, I think we need to evaluate that scenario as a minimum, assuming the crowd is leaving such an event at a time coinciding with a busy period for GBZ activities (eg weekend midday or mid-afternoon).

## Comment:

The large events at Pukekohe Park are considered to be infrequent events and are required to be under control of Traffic Management Plans. It should also be noted that the Pukekohe Paerata Structure Plan has identified this area as an area for employment growth to support residential development in Pukekohe and this location is seen as an ideal place to establish employment related activities.

It is however acknowledged that events under 5000 people do not require a TMP. In terms of context:

- The original 2018 Saturday survey date was especially chosen as Counties Cup day, which from discussion with Counties Racing is currently the busiest day (around 3,500-5000 people).
- In the next 12 months a total of nine "events" are planned at the Racecourse (generally running November to March)
- If these 8 will occur on a Saturday. Given the start and end times of these events (starting at 11am) they most likely crossover is people arriving for the event early afternoon on a Saturday coinciding with retail customers peak.
- Information from Pukekohe Park has the "Counties Cup" as the Largest Horse Racing meeting and has had between 3-5000 over past years. For this event, a number of hospitality area patrons use buses and thus they typically have 10-12 buses onsite for the larger events.

As such having an event at around 5000 people on a Saturday afternoon without needing a TMP is considered a very rare event (maybe once a year at most).

The trip generation has been reviewed based on likely mode split as follows:

- 5,000 people
- Based on the survey information 33\% arrive in one peak hour (noting the events tend to last for $6+$ hours). This peak hour is assumed to be the same retail peak hour as a worst case.
- $75 \%$ arrive by car ( $50 \%$ in private car and $25 \%$ drop off such as taxi / uber)
- $20 \%$ by bus
- $5 \%$ other (walking / cycling)
- Average occupancy of 3 people per vehicle for private car, 2 people for uber, 50 for bus.
- Private car has all cars entering, taxi creates two trips (one entering, one exiting)
- Trip generation of 632 vehicles per hour.
- These vehicles likely to be split over the three entry gates, with the key gate 2 and 3 assumed to cater for $80 \%$ of the traffic ( $40 \%$ each) or 252 vph (177 in 75 out)

The 2018 survey as contained in the ITA has a total of 259 vehicles per hour in the peak at Gate 3 (211 in and 48 out). As such the surveyed Raceday is similar to the theoretical model split analysis and all Saturday modelling provided thus already considers a larger horse race event.

As such every other Saturday throughout the year will likely perform significantly better than the modelling results show as the other Horse Racing events will likely be smaller is size (or most likely not occur at all) and the motor racing will also no longer occur ${ }^{1}$.

## 3 ITEM T22: PEDESTRIANS/ CYCLISTS

You have indicated that the roundabouts would have pedestrian crossings on all approaches in line with AT guidance. The AT guidance shows zebra crossings on raised tables which would have a significant effect on the saturation flows at the roundabout and reduce the intersection capacity significantly. I think this aspect needs some additional investigation.

## Comment:

We agree with the comment that zebra crossings at the roundabout would potentially reduce capacity at the roundabout. However, in terms of the Plan Change crossing facilities:

[^0]- The exact pedestrian location / design can only be determined at future stages when lot / building layouts are known and thus pedestrian desire lines are able to be determined.
- As such the exact level of effect of pedestrians on the performance of the roundabout is difficult to accurately replicate at Plan Change level.
- Again, it is noted that all the above would be subject to further detailed design / Auckland Transport approval.
- The option of a signalised intersection at the Kitchener Road / Manukau Road intersection as modelled does have pedestrian phases included.
- There is the potential of a mid-block signalised pedestrian crossing.


## Yours sincerely

## Commute Transportation Consultants

## Leo Hills



## Director

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## MOVEMENT SUMMARY

$\theta$ Site: 102v [Manukau Rd/ Kitchener Rd/ Buckland Rd intersection Proposed SAT - 100\% Ifr 15\%]
New Site
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Buckland Rd (south) |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 82 | 5.0 | 1.149 | 156.3 | LOS F | 117.2 | 855.9 | 1.00 | 4.14 | 17.1 |
| 2 | T1 | 965 | 5.0 | 1.149 | 156.4 | LOS F | 117.2 | 855.9 | 1.00 | 4.14 | 17.3 |
| 3 | R2 | 47 | 5.0 | 1.149 | 162.1 | LOS F | 117.2 | 855.9 | 1.00 | 4.14 | 17.3 |
| Appr | ch | 1095 | 5.0 | 1.149 | 156.6 | LOS F | 117.2 | 855.9 | 1.00 | 4.14 | 17.2 |
| East: Gate 2 (site main access) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 31 | 5.0 | 0.873 | 63.9 | LOS E | 14.7 | 107.0 | 1.00 | 1.51 | 29.0 |
| 5 | T1 | 69 | 5.0 | 0.873 | 64.1 | LOS E | 14.7 | 107.0 | 1.00 | 1.51 | 29.5 |
| 6 | R2 | 196 | 5.0 | 0.873 | 69.7 | LOS E | 14.7 | 107.0 | 1.00 | 1.51 | 29.6 |
| Appro | ch | 296 | 5.0 | 0.873 | 67.8 | LOS E | 14.7 | 107.0 | 1.00 | 1.51 | 29.5 |
| North: Manukau Rd (north) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 327 | 5.0 | 1.136 | 134.3 | LOS F | 152.7 | 1114.6 | 1.00 | 3.10 | 18.9 |
| 8 | T1 | 953 | 5.0 | 1.136 | 134.5 | LOS F | 152.7 | 1114.6 | 1.00 | 3.10 | 19.1 |
| 9 | R2 | 221 | 5.0 | 1.136 | 140.2 | LOS F | 152.7 | 1114.6 | 1.00 | 3.10 | 19.2 |
| Appr |  | 1501 | 5.0 | 1.136 | 135.3 | LOS F | 152.7 | 1114.6 | 1.00 | 3.10 | 19.1 |
| West: Kitchener Rd (west) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 334 | 5.0 | 1.312 | 328.9 | LOS F | 93.8 | 684.9 | 1.00 | 4.00 | 9.4 |
| 11 | T1 | 93 | 5.0 | 1.312 | 329.0 | LOS F | 93.8 | 684.9 | 1.00 | 4.00 | 9.5 |
| 12 | R2 | 74 | 5.0 | 1.312 | 334.7 | LOS F | 93.8 | 684.9 | 1.00 | 4.00 | 9.5 |
| Approach |  | 500 | 5.0 | 1.312 | 329.8 | LOS F | 93.8 | 684.9 | 1.00 | 4.00 | 9.4 |
| All Ve | cles | 3392 | 5.0 | 1.312 | 165.0 | LOS F | 152.7 | 1114.6 | 1.00 | 3.43 | 16.6 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## $\theta$ Site: 102v [Manukau Rd/ PPC Road intersection SAT - 100\% +15\%]

New Site
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. <br> Satn <br> v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | of Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Buckland Rd (south) |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 246 | 5.0 | 1.127 | 146.4 | LOS F | 80.3 | 586.3 | 1.00 | 3.50 | 17.7 |
| 2 | T1 | 522 | 5.0 | 1.127 | 146.7 | LOS F | 80.3 | 586.3 | 1.00 | 3.50 | 17.8 |
| 3 | R2 | 11 | 5.0 | 1.127 | 151.4 | LOS F | 80.3 | 586.3 | 1.00 | 3.50 | 17.8 |
| Appr |  | 779 | 5.0 | 1.127 | 146.7 | LOS F | 80.3 | 586.3 | 1.00 | 3.50 | 17.8 |
| East: Gate 3 |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 11 | 5.0 | 0.138 | 23.1 | LOS C | 1.1 | 7.9 | 1.00 | 0.91 | 42.5 |
| 5 | T1 | 11 | 5.0 | 0.138 | 23.4 | LOS C | 1.1 | 7.9 | 1.00 | 0.91 | 43.3 |
| 6 | R2 | 11 | 5.0 | 0.138 | 28.0 | LOS C | 1.1 | 7.9 | 1.00 | 0.91 | 43.2 |
| Appr |  | 32 | 5.0 | 0.138 | 24.8 | LOS C | 1.1 | 7.9 | 1.00 | 0.91 | 43.0 |
| North: Bucklend Rd (north) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 11 | 5.0 | 0.980 | 31.7 | LOS C | 42.6 | 310.8 | 1.00 | 1.39 | 38.4 |
| 8 | T1 | 482 | 5.0 | 0.980 | 32.0 | LOS C | 42.6 | 310.8 | 1.00 | 1.39 | 39.1 |
| 9 | R2 | 575 | 5.0 | 0.980 | 36.7 | LOS D | 42.6 | 310.8 | 1.00 | 1.39 | 39.0 |
| Appr |  | 1067 | 5.0 | 0.980 | 34.5 | LOS C | 42.6 | 310.8 | 1.00 | 1.39 | 39.0 |
| West: PPC Road |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 575 | 5.0 | 1.031 | 71.5 | LOS F | 51.7 | 377.5 | 1.00 | 2.34 | 27.3 |
| 11 | T1 | 11 | 5.0 | 1.031 | 71.8 | LOS F | 51.7 | 377.5 | 1.00 | 2.34 | 27.6 |
| 12 | R2 | 246 | 5.0 | 1.031 | 76.5 | LOS F | 51.7 | 377.5 | 1.00 | 2.34 | 27.6 |
| Approach |  | 832 | 5.0 | 1.031 | 73.0 | LOS F | 51.7 | 377.5 | 1.00 | 2.34 | 27.4 |
| All Vehicles |  | 2709 | 5.0 | 1.127 | 78.5 | LOS F | 80.3 | 586.3 | 1.00 | 2.28 | 26.5 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: SIDRA Roundabout LOS.
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
Roundabout Capacity Model: SIDRA Standard.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

日 Site: 102vv [Manukau Rd/ Kitchener Rd/ Buckland Rd intersection Proposed SAT - 100\% Ifr - signals +15\%]

New Site
Signals - Fixed Time Isolated Cycle Time $=150$ seconds (Practical Cycle Time)

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov ID | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Deman Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | f Queue Distance m | Prop. Queued | Effective Stop Rate per veh | Average Speed km/h |
| South: Buckland Rd (south) |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 82 | 5.0 | 0.077 | 19.2 | LOS B | 2.5 | 18.1 | 0.45 | 0.68 | 44.6 |
| 2 | T1 | 965 | 5.0 | 0.808 | 49.4 | LOS D | 35.2 | 256.7 | 0.95 | 0.87 | 33.1 |
| 3 | R2 | 47 | 5.0 | 0.209 | 69.7 | LOS E | 3.2 | 23.0 | 0.94 | 0.75 | 27.6 |
| Appr | ch | 1095 | 5.0 | 0.808 | 48.0 | LOS D | 35.2 | 256.7 | 0.92 | 0.85 | 33.5 |
| East: Gate 2 (site main access) |  |  |  |  |  |  |  |  |  |  |  |
| 4 | L2 | 31 | 5.0 | 0.052 | 42.1 | LOS D | 1.5 | 10.9 | 0.71 | 0.70 | 34.9 |
| 5 | T1 | 69 | 5.0 | 0.979 | 105.2 | LOS F | 25.1 | 183.3 | 1.00 | 1.12 | 21.5 |
| 6 | R2 | 196 | 5.0 | 0.979 | 110.9 | LOS F | 25.1 | 183.3 | 1.00 | 1.12 | 21.4 |
| Appr | ch | 296 | 5.0 | 0.979 | 102.4 | LOS F | 25.1 | 183.3 | 0.97 | 1.07 | 22.3 |
| North: Manukau Rd (north) |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 327 | 5.0 | 0.490 | 18.4 | LOS B | 8.8 | 64.0 | 0.65 | 0.76 | 45.0 |
| 8 | T1 | 953 | 5.0 | 0.957 | 82.0 | LOS F | 55.5 | 405.3 | 0.95 | 1.09 | 25.5 |
| 9 | R2 | 221 | 5.0 | 0.973 | 109.8 | LOS F | 20.6 | 150.6 | 1.00 | 1.04 | 21.2 |
| Appr |  | 1501 | 5.0 | 0.973 | 72.2 | LOS E | 55.5 | 405.3 | 0.89 | 1.01 | 27.3 |
| West: Kitchener Rd (west) |  |  |  |  |  |  |  |  |  |  |  |
| 10 | L2 | 334 | 5.0 | 0.710 | 29.1 | LOS C | 12.7 | 92.7 | 0.86 | 0.81 | 39.8 |
| 11 | T1 | 93 | 5.0 | 0.961 | 98.5 | LOS F | 14.7 | 107.0 | 0.91 | 1.07 | 22.7 |
| 12 | R2 | 74 | 5.0 | 0.961 | 104.2 | LOS F | 14.7 | 107.0 | 0.91 | 1.07 | 22.5 |
| Approach |  | 500 | 5.0 | 0.961 | 53.0 | LOS D | 14.7 | 107.0 | 0.88 | 0.90 | 31.7 |
| All Vehicles |  | 3392 | 5.0 | 0.979 | 64.2 | LOS E | 55.5 | 405.3 | 0.91 | 0.95 | 29.0 |

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Vehicle movement LOS values are based on average delay per movement.
Intersection and Approach LOS values are based on average delay for all vehicle movements.
SIDRA Standard Delay Model is used. Control Delay includes Geometric Delay.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Movement Performance - Pedestrians

| Mov ID | Description | Demand Flow ped/h | Average Delay sec | Level of Service | Average Back Pedestrian ped | of Queue Distance m | Prop. Queued | Effective Stop Rate per ped |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P1 | South Full Crossing | 53 | 68.3 | LOS F | 0.2 | 0.2 | 0.96 | 0.96 |
| P2 | East Full Crossing | 53 | 39.0 | LOS D | 0.2 | 0.2 | 0.72 | 0.72 |
| P3 | North Full Crossing | 53 | 60.9 | LOS F | 0.2 | 0.2 | 0.90 | 0.90 |
| P4 | West Full Crossing | 53 | 39.0 | LOS D | 0.2 | 0.2 | 0.72 | 0.72 |
| All Pe | estrians | 211 | 51.8 | LOS E |  |  | 0.83 | 0.83 |

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.


[^0]:    1 https://i.stuff.co.nz/sport/motorsport/300641696/motorsport-to-end-at-pukekohe-raceway-after-60-years-making-way-for-horse-racing

