

WASTE WATER AND PIPE FLOW CALCULATOR

WATERCARE WASTEWATER CODE OF PRACTICE - COLEBROOK WHITE AND MANNINGS EQUATIONS

CLIENT:	Hugh Green Group
PROJECT:	Park Estate Road Overall Catchment
DETAIL:	Scenario 1 - Currently Developed

DESIGNER:	RGP
JOB NO:	1972-00
DATE:	18/05/2021
REV:	2

NOTE: This spreadsheet calculates peak flow rates using the Watercare Code of Practice and pipe capacities using the Colebrook-White equation for pipes flowing full, and the Mannings equation for pipes flowing part-full

Green boxes are user inputs

Design Flow Assumptions (Section 5.3.5.1 WWCoP):

Residential	Residential	High Rise Residential		
Average Dry Weather Flow (ADWF) =	180	180	I/p/d	
Peak Factor: Self-Cleansing Design Flow =	3.0	3.0		
Peak Factor: Peak Design Flow =	6.7	5.0		
Self-Cleansing Design Flow (ADWF) =	540.0	540.0	I/p/d	
Peak Design Flow (PWWF) =	1206.0	900.0	I/p/d	
Number of People per Dwelling =	3.0	5.0	p	
Commercial/Industrial	Design Flow (l/m ² /d)	ADWF (l/m ² /d)	PWWF (l/m ² /d)	
Dry retail (toilets not available to customers)	1.3	2.6	6.5	
Dry retail (toilets available to customers) / Office Buildings	4.3	8.6	21.5	
Wet retail (food and beverage retail/preparation)	15.0	30	100.5	
Industrial: light water use	4.5	22.5	30.2	
Industrial: medium water use	6.0	30	40.2	
Industrial: heavy water use	11.0	55	73.7	
Very heavy water users	Specific Design Required			
Commercial/Industrial Selected Values =	1.3	2.6	6.5	
Other Facility Types	Refer to table, WWCoP pg 33			
Peak Factor: Self-Cleansing Design Flow =	2			
Peak Factor: Peak Design Flow =	6.7			

Table 5.2 – Guide to roughness coefficients for wastewater lines

Material	Colebrook-White coefficient k (mm)	Manning roughness coefficient (n)
All pipe material and lining types for gravity systems and low pressure collection systems (PWC), flowing full.	1.5	0.013
All pipe material and lining types for pressure rising mains, flowing full	0.6	0.011
NOTE – (1.) These values take into account possible effects of rubber ring joints, slime, and debris. (2.) The n and k values apply for pipes up to and including DN 300.		

Table 5.3 – Minimum pipe sizes for wastewater reticulation and property connections

Pipe	Minimum size DN (mm)
Connection servicing 1 dwelling unit	100
Connection servicing more than 1 dwelling unit	150
Connection servicing commercial lots	150
Connection servicing industrial lots	225
NOTE – In practical terms, in a residential development not exceeding 20 dwelling units, and where no pumping station is involved, DN 150 pipes laid within the limits of table 5.4 and table 5.5 will be adequate without specific hydraulic design of the pipe network.	

Line	Catchment Details	Increment Number of Residential/ Rural Dwellings	Increment Number of High Density Dwellings	Increment Commercial/ Industrial Area (m ²)	Increment Other Facility Type (l/d)	Increment ADWF (l/s)	Cumulative ADWF (l/s)	Increment PDWF (l/s)	Cumulative PDWF (l/s)	Increment PWWF (l/s)	Cumulative PWWF (l/s)	Household Unit Equivalent	Diam (mm)	Ks	n	Grade (%)	Qmax (l/s)	Velocity Flowing Full (m/s)	Check Capacity - % of Qpwwf vs Qmax (must be <100%)	Vpdwf (must be >0.75m/s for self cleansing)	Check flow depth in pipe while carrying PDWF (must be < 50%)
EXISTING (Existing conditions including Hugh Green Development stages 1A - 1D and MOE)	Refer to sketch plan 1972-00-SK41-1 and 1972-00-SK41-2 for catchment boundaries																				
PUMPED CATCHMENT																					
SSMH 7 - SSMH 6	Pumped flows from upstream of Hugh Green Development	3087				19.3	19.3	57.9	57.9	129.3	129.3	3087	450	1.500	0.013	0.72	243	1.53	53.1%	1.20	34.3%
SSMH 6 - SSMH 5						0.0	19.3	0.0	57.9	0.0	129.3	0	450	1.500	0.013	0.67	235	1.48	55.0%	1.17	34.9%
SSMH 5 - SSMH 4						0.0	19.3	0.0	57.9	0.0	129.3	0	450	1.500	0.013	0.73	245	1.54	52.7%	1.21	34.1%
SSMH 4 - SSMH 3						0.0	19.3	0.0	57.9	0.0	129.3	0	450	1.500	0.013	0.64	230	1.44	56.3%	1.15	35.3%
SSMH 3 - SSMH 2						0.0	19.3	0.0	57.9	0.0	129.3	0	525	1.500	0.013	0.31	240	1.11	53.9%	0.88	34.4%
SSMH 2 - SSMH 1						0.0	19.3	0.0	57.9	0.0	129.3	0	525	1.500	0.013	0.22	202	0.93	64.1%	0.78	37.7%
GRAVITY FED CATCHMENT	Assumes pumped catchment flows are off peak																				
SSMH 7 - SSMH 6	Gravity fed flows from upstream of Hugh Green Developments	1000			15820	6.4	6.4	19.1	19.1	43.1	43.1	1026	450	1.500	0.013	0.72	243	1.53	17.7%	0.88	19.5%
SSMH 6 - SSMH 5	Gravity fed flows from Hugh Green	30			12825	0.3	6.8	0.9	20.0	2.3	45.4	51	450	1.500	0.013	0.67	235	1.48	19.3%	0.87	20.3%
SSMH 5 - SSMH 4	Developments Stages 1a - 1d and Stage	77				0.5	7.3	1.4	21.4	3.2	48.6	77	450	1.500	0.013	0.73	245	1.54	19.8%	0.91	20.5%
SSMH 4 - SSMH 3	MOE	51				0.3	7.6	1.0	22.4	2.1	50.7	51	450	1.500	0.013	0.64	230	1.44	22.1%	0.88	21.7%
SSMH 3 - SSMH 2						0.0	7.6	0.0	22.4	0.0	50.7	0	525	1.500	0.013	0.31	240	1.11	21.2%	0.67	21.2%
SSMH 2 - SSMH 1						0.0	7.6	0.0	22.4	0.0	50.7	0	525	1.500	0.013	0.22	202	0.93	25.1%	0.59	23.1%
Combined Catchment Flow							26.9		80.3		180.0		525	1.500	0.013	0.22	202	0.93	89.2%	0.86	44.8%
1. Pumped Cumulative flows assume all flows are pumped simultaneously																					

Notes/Conclusions

Combined pumped and gravity fed flows do not exceed capacity therefore ok

WASTE WATER AND PIPE FLOW CALCULATOR

WATERCARE WASTEWATER CODE OF PRACTICE - COLEBROOK WHITE AND MANNINGS EQUATIONS

CLIENT:	Hugh Green Group
PROJECT:	Park Estate Road Overall Catchment
DETAIL:	Scenario 2 - MPD Development before plan change

DESIGNER:	RGP
JOB NO:	1972-00
DATE:	18/05/2021
REV:	2

NOTE: This spreadsheet calculates peak flow rates using the Watercare Code of Practice and pipe capacities using the Colebrook-White equation for pipes flowing full, and the Mannings equation for pipes flowing part-full

Green boxes are user inputs

Design Flow Assumptions (Section 5.3.5.1 WWCoP):

Residential	Residential	High Rise Residential	
Average Dry Weather Flow (ADWF) =	180	180	l/p/d
Peak Factor: Self-Cleansing Design Flow =	3.0	3.0	
Peak Factor: Peak Design Flow =	6.7	5.0	
Self-Cleansing Design Flow (ADWF) =	540.0	540.0	l/p/d
Peak Design Flow (PWWF) =	1206.0	900.0	l/p/d
Number of People per Dwelling =	3.0	5.0	p
Commercial/Industrial	Design Flow (l/m ² /d)	ADWF (l/m ² /d)	PWWF (l/m ² /d)
Dry retail (toilets not available to customers)	1.3	2.6	6.5
Dry retail (toilets available to customers) / Office Buildings	4.3	8.6	21.5
Wet retail (food and beverage retail/preparation)	15.0	30	100.5
Industrial: light water use	4.5	22.5	30.2
Industrial: medium water use	6.0	30	40.2
Industrial: heavy water use	11.0	55	73.7
Very heavy water users	Specific Design Required		
Commercial/Industrial Selected Values =	1.3	2.6	6.5
Other Facility Types	Refer to table, WWCoP pg 33		
Peak Factor: Self-Cleansing Design Flow =	2		
Peak Factor: Peak Design Flow =	6.7		

Table 5.2 – Guide to roughness coefficients for wastewater lines

Material	Colebrook-White coefficient k (mm)	Manning roughness coefficient (n)
All pipe material and lining types for gravity systems and low pressure collection systems (PWC), flowing full.	1.5	0.013
All pipe material and lining types for pressure rising mains, flowing full	0.6	0.011
NOTE – (1.) These values take into account possible effects of rubber ring joints, slime, and debris. (2.) The n and k values apply for pipes up to and including DN 300.		

Table 5.3 – Minimum pipe sizes for wastewater reticulation and property connections

Pipe	Minimum size DN (mm)
Connection servicing 1 dwelling unit	100
Connection servicing more than 1 dwelling unit	150
Connection servicing commercial lots	150
Connection servicing industrial lots	225
NOTE – In practical terms, in a residential development not exceeding 20 dwelling units, and where no pumping station is involved, DN 150 pipes laid within the limits of table 5.4 and table 5.5 will be adequate without specific hydraulic design of the pipe network.	

Line	Catchment Details	Increment Number of Residential/ Rural Dwellings	Increment Number of High Density Dwellings	Increment Commercial/ Industrial Area (m²)	Increment Other Facility Type (l/d)	Increment ADWF (l/s)	Cumulative ADWF (l/s)	Increment PDWF (l/s)	Cumulative PDWF (l/s)	Increment PWWF (l/s)	Cumulative PWWF (l/s)	Household Unit Equivalent	Diam (mm)	Ks	n	Grade (%)	Qmax (l/s)	Velocity Flowing Full (m/s)	Check Capacity - % of Qpwwf vs Qmax (must be <100%)	Vpdwf (must be >0.75m/s for self cleansing)	Check flow depth in pipe while carrying PDWF (must be < 50%)
FUTURE (Flows from entire catchment area calculated at MPD)	Refer to sketch plan 1972-00-SK41-1 and 1972-00-SK41-2 for catchment boundaries																				
PUMPED CATCHMENT																					
SSSMH 7 - SSMH 6	Pumped flows from upstream of Hugh Green Development	5268	18		32680	33.5	33.5	100.1	100.1	224.1	224.1	5340	450	1500	0.013	0.72	243	1.53	92.0%	1.41	45.7%
SSSMH 6 - SSMH 5						0.0	33.5	0.0	100.1	0.0	224.1	0	450	1500	0.013	0.67	235	1.48	95.4%	1.38	46.6%
SSSMH 5 - SSMH 4						0.0	33.5	0.0	100.1	0.0	224.1	0	450	1500	0.013	0.73	245	1.54	91.4%	1.42	45.5%
SSSMH 4 - SSMH 3						0.0	33.5	0.0	100.1	0.0	224.1	0	450	1500	0.013	0.64	230	1.44	97.6%	1.36	47.2%
SSSMH 3 - SSMH 2						0.0	33.5	0.0	100.1	0.0	224.1	0	525	1500	0.013	0.31	240	1.11	93.5%	1.03	46.0%
SSSMH 2 - SSMH 1						0.0	33.5	0.0	100.1	0.0	224.1	0	525	1500	0.013	0.22	202	0.93	111.1%	0.91	50.5%
GRAVITY FED CATCHMENT																					
SSSMH 7 - SSMH 6	Assumes pumped catchment flows are off peak																				
SSSMH 7 - SSMH 6	Gravity fed flows from upstream of Hugh Green Developments	3226			66890	20.9	20.9	62.0	62.0	140.3	140.3	3337	450	1500	0.013	0.72	243	1.53	57.6%	1.23	35.5%
SSSMH 6 - SSMH 5	Gravity fed flows from fully complete Hugh Green Developments	102			12825	0.8	21.7	2.2	64.2	5.3	145.5	123	450	1500	0.013	0.67	235	1.48	62.0%	1.21	36.8%
SSSMH 5 - SSMH 4		233				1.5	23.2	4.4	68.6	9.8	155.3	233	450	1500	0.013	0.73	245	1.54	63.3%	1.27	37.3%
SSSMH 4 - SSMH 3		237				1.5	24.7	4.4	73.1	9.9	165.2	237	450	1500	0.013	0.64	230	1.44	72.0%	1.23	39.9%
SSSMH 3 - SSMH 2		370				2.3	27.0	6.9	80.0	15.5	180.7	370	525	1500	0.013	0.31	240	1.11	75.4%	0.96	40.8%
SSSMH 2 - SSMH 1		48					0.3	27.3	0.9	80.9	2.0	182.7	48	525	1500	0.013	0.22	202	0.93	90.6%	0.86
Combined Catchment Flow							60.8		181.0		406.8		525	1500	0.013	0.22	202	0.93	201.6%	1.07	72.6%
1. Future catchment areas are calculated according to Auckland Unitary Plan at Maximum Probable Development.																					
2. Pumped Cumulative flows assume all flows are pumped simultaneously																					

Notes/Conclusions

Combined pumped and gravity fed flows exceed capacity therefore pumped flows must be off peak

WASTE WATER AND PIPE FLOW CALCULATOR

WATERCARE WASTEWATER CODE OF PRACTICE - COLEBROOK WHITE AND MANNINGS EQUATIONS

CLIENT:	Hugh Green Group
PROJECT:	Park Estate Road Overall Catchment
DETAIL:	Scenario 3 - MPD Development after plan change

DESIGNER:	RGP
JOB NO:	1972-00
DATE:	18/05/2021
REV:	2

NOTE: This spreadsheet calculates peak flow rates using the Watercare Code of Practice and pipe capacities using the Colebrook-White equation for pipes flowing full, and the Mannings equation for pipes flowing part-full

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Very heavy water users	Specific Design Required		
Commercial/Industrial Selected Values =	1.3	2.6	6.5
Other Facility Types	Refer to table, WWCoP pg 33		
Peak Factor: Self-Cleansing Design Flow =	2		
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SSSMH 4 - SSMH 3						0.0	33.5	0.0	100.1	0.0	224.1	0	450	1500	0.013	0.64	230	1.44	97.6%	1.36	47.2%
SSSMH 3 - SSMH 2						0.0	33.5	0.0	100.1	0.0	224.1	0	525	1500	0.013	0.31	240	1.11	93.5%	1.03	46.0%
SSSMH 2 - SSMH 1						0.0	33.5	0.0	100.1	0.0	224.1	0	525	1500	0.013	0.22	202	0.93	111.1%	0.91	50.5%
GRAVITY FED CATCHMENT																					
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SSSMH 5 - SSMH 4		233				1.5	23.2	4.4	68.6	9.8	155.3	233	450	1500	0.013	0.73	245	1.54	63.3%	1.27	37.3%
SSSMH 4 - SSMH 3		237				1.5	24.7	4.4	73.1	9.9	165.2	237	450	1500	0.013	0.64	230	1.44	72.0%	1.23	39.9%
SSSMH 3 - SSMH 2		590				3.7	28.3	11.1	84.1	24.7	189.9	590	525	1500	0.013	0.31	240	1.11	79.2%	0.98	41.9%
SSSMH 2 - SSMH 1		55					0.3	28.7	1.0	85.2	2.3	192.2	55	525	1500	0.013	0.22	202	0.93	95.3%	0.87
Combined Catchment Flow							62.2		185.2		416.3		525	1500	0.013	0.22	202	0.93	206.3%	1.08	74.0%
1. Future catchment areas are calculated according to Auckland Unitary Plan at Maximum Probable Development.																					
2. Pumped Cumulative flows assume all flows are pumped simultaneously																					

Notes/Conclusions

Combined pumped and gravity fed flows exceed capacity therefore pumped flows must be off peak

