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GEOTECHNICAL INVESTIGATION REPORT PROPOSED NEW SUBDIVISION 278 CLEVEDON-KAWAKAWA ROAD **CLEVEDON**

Prepared For:

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REPORT ISSUE AUTHORISATION

Geotechnical Investigation Report Proposed New Subdivision 278 Clevedon-Kawakawa Road Clevedon

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EXECUTIVE SUMMARY

Geotechnical Investigation Report Proposed New Subdivision 278 Clevedon-Kawakawa Road Clevedon

	Geology	Tauranga Group Alluvium		
SUBSOIL	Lithology	Clayey SILT / Silty CLAY, sandy SILT / Silty SAND with minor fine to medium gravels		
CONDITIONS (See borehole logs for	Groundwater depth	Between 1.3m and 3.8m below ground level		
details)	Shrink/swell classification (AS2870:2011)	Class 'M' (moderately reactive)		
	Soil classification as per NZS 1170.5:2004	Class 'C'		
SITE STABILITY COMMENT	 Provided the recommendations in section 12 are followed, slope stability is not considered a concern for the site. 			
SITE FORMATION CONSTRAINTS	 Provided that excavations no greater than 0.5m are undertaken within natural soils, they are expected to be temporarily stable. All excavations are recommended to be covered with GAP20 or similar hardfill to prevent the soils from drying out. 			
FOUNDATION RECOMMENDATIONS (see Section 12 for complete text)	 Provided that the structure is located a minimum of 4.5m away from the edge of slopes with gradients 1:4 or steeper, an NZS 3604:2011 type structure, founded on conventional shallow foundations is considered to be appropriate. For shallow foundations, an ultimate unfactored bearing capacity of 300kPa may be adopted. Where the building platforms are located within 4.5m of slopes with gradients 1:4 or steeper or comprises heavy construction materials, specific geotecnical engineering input is required. 			
REPORT DISTRIBUTION	A full copy of this report must be provided to all relevant parties involved in the project. This should include, but not be limited to, owner, architectural designers, engineers (civil and structural) and the earthworks/building contractor.			



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Appendix B:	Subsurface Investigation Records (Hand Auger Boreholes and
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1. INTRODUCTION

At the instruction of Stratford Properties Limited, we have carried out a geotechnical engineering investigation for a proposed residential subdivision at 278 Clevedon-Kawakawa Road, Clevedon. The scope of our investigation was to conduct a detailed site walkover inspection and to explore subsurface conditions using hand operated equipment and cone penetrometer testing. The information obtained has been used to assess ground conditions, review site stability, determine the presence of a safe and stable building platforms and access to it and provide preliminary geotechnical considerations for future development.

This report presents our findings and conclusions and has been prepared in support of a Resource Consent application.

2. SITE DESCRIPTION

No. 278 Clevedon Kawakawa Road, Clevedon is legally described as Lot 1 DP 146882 and has a total plan area of 51.7 ha. The Lot is approximately rectangular in shape, and is located to the south of Wairoa River and to the north of Clevedon-Kawakawa Road, with access via a private driveway from no 272 Clevedon-Kawakawa Road. The site is bound to the east and west by farm land properties.

The proposed development area (herein referred to as 'the site') is located within the southern portion of the property, towards Clevedon-Kawakawa Road, where an irregular shaped raised knoll and an elevated strip along the road front are located. The strip along the road front slopes gently to the north reaching a maximum gradient of 1 Vertical on 10 Horizontal (1V:10H). The surface of the raised knoll, which is located approximately 200m north of the road is relatively flat to gently sloping with the sides of the knoll gently to steeply sloping reaching a maximum gradient of 1V:3H.

The site consists almost entirely of open green pastures with some minor bushes and trees located along the southern fence line. The surrounding low lying areas below the knoll and southern strip have all been designated as flood plains, truncated by several overland flow paths.

The property is not currently serviced by a public stormwater or sewer network. An indication of the current topography and existing features is shown on the Site Plan (Sheet 1).



3. PROPOSED DEVELOPMENT

Drawings provided to us by Greenwood Associates titled "Stratford Properties - 278 Clevedon-Kawakawa Road Clevedon, Auckland" drawing No. 912/1 and 912/2 dated 14 January 2019 (Appendix A) detail a proposed residential subdivision which will have individual onsite waste water disposal fields. Lot boundaries had not been confirmed at the time of preparing this report, however we understand that there will be in the order of 11 to 12 Lots proposed across 'the site'. A new shared accessway is also proposed off Clevedon-Kawakawa Road with private driveways off the main accessway providing access to each property.

4. BACKGROUND INFORMATION AND SITE OBSERVATIONS

4.1 Historical Site Development

An assessment of aerial photographs between 1940 and 2017 indicate the site has undergone very little to no development since 1940, with the site primarily used for grazing for livestock.

4.2 Site Reconnaissance

During our site reconnaissance we have noted the following;

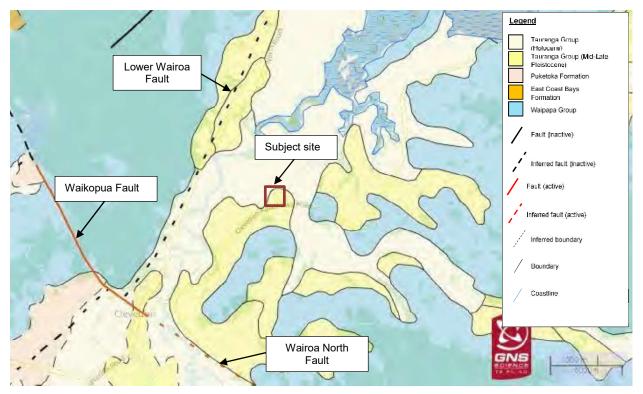
- The topography raises gently to moderately along the west, south and southeastern edges of the knoll but to the north and northeast the slope dips moderately to steeply.
- The slope to the north of the knoll has clear indicators of some previous surficial failure movements.
- The proposed development area along the top of the knoll is nearly flat to gently sloping.
- The development area adjacent to Clevedon-Kawakawa Road is gently sloping to the north.
- A number of shallow stormwater trenches are visible in the low lying areas of 278 Clevedon-Kawakawa Road.
- A number of reeds/tall grasses are visible in the low lying areas suggesting groundwater may be shallow at places.
- The overland flow paths are generally present in the low lying areas and between the development sites

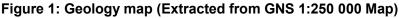


5. GEOLOGY

The regional geology of the site and its surrounding area is detailed on the Geological Map of the Auckland Area Sheet 3 of the Geological Map Series (Scale 1:250,000), published by the institute of Geological and Nuclear Sciences in 2001. This shows the site to be underlain by pumiceous sand, silt, and clay, with interbedded gravel and peat associated with the Taranga Group of Pleistocene and Holocene age. Therefore, it is anticipated that the superficial deposits will comprise predominately alluvial deposits of the Tauranga Group.

Three major published faults, the Lower Wairoa Fault, the Waikopua Fault and the Wairoa North Fault are located around the proposed development site. The Lower Wairoa Fault is located approximately 1km to the northwest of the proposed site and dips to the southeast with information provided from GNS Geoscience website indicating the fault is currently inactive. The Waikopua and Wairoa North Fault are located approximately 2.5km and 2.3km to the southwest respectively and dip to the southwest with information provided from GNS Geoscience website indicating the fault section. During our site reconnaissance, though some minor surficial surface movement of the soils were observed, no evidence of any major fault movements was observed over the proposed site development area







6. FIELD EXPLORATION

6.1 Hand Auger Boreholes

The subsurface conditions at the site were explored by drilling 8 no. hand auger boreholes (AH1 to AH8) on 14, 15 and 18 February 2019, at the locations shown on our Site Plan. The subsurface conditions encountered during drilling were logged in general accordance with 'The guidelines for the classification and description of soil and rock for engineering purposes', December 2005 as outlined by the NZ Geotechnical Society Guidelines.

A calibrated shear vane, used in accordance with New Zealand Geotechnical Society Guideline for Hand Held Shear Vane Test, 2001 was used at regular depths in the drilled holes to measure soil strengths, both in situ and remoulded. The vane shear strengths shown on the attached logs have been corrected in terms of BS 1377.

Scala penetrometer testing was subsequently undertaken through the base of each borehole with a view to establishing a general indication of soil resistance for a further 2m beyond the base of each borehole, or until effective refusal was encountered, whichever being encountered first.

The site was subsequently revisited on 19 February 2019 in order to check for standing groundwater after the effects of drilling had dissipated. Where encountered, the measured depths to standing groundwater level are marked on the relevant borehole logs.

6.2 Cone Penetration Test (CPT)

Two CPTs (CPT1 and CPT2) were undertaken by Ground Investigation Limited on 14 February 2019. The CPTs were intended to be advanced to a depth of 20m below present ground level, or until effective refusal, whichever was encountered first. The primary purpose of the probes was to provide information on the ground profile and provide data for liquefaction analysis.

The CPTs were undertaken with a 1 tonne Pagani TG63-150 rig, using a cone with a cross-sectional area of 10cm². Continuous measurements of pore pressures were undertaken during testing. The tests were undertaken in accordance with ASTM Standard 5778-12 procedure.



7. SUBSURFACE CONDITIONS

The subsurface ground conditions encountered in each borehole and CPT are briefly described and summarised below in Table 1. For details of particular investigations, reference should be made to the attached investigation logs in Appendix B as shown on the Site Plan. Where CPT probes were undertaken, they did not return any samples. However, inferences have been drawn from the results to the materials logged in nearby investigation points Subsoil conditions have been interpolated between the boreholes and the CPTs. It must be accepted that soil conditions are inherently variable and no investigation can be exhaustive to the extent that all soil conditions are revealed. A representative site specific geological cross section is attached as Sheet 2 and 3.

The following is the general description of the materials encountered:

7.1 Topsoil

A surface veneer of topsoil up to approximately 0.3m was encountered in all boreholes and was found to comprise typical organic topsoil materials. Topsoil is expected to be continuous across the site, not including paved areas, however, it must be appreciated that topsoil thicknesses may vary across the site. No shear vane readings were taken within this material.

7.2 Tauranga Group Alluvium - Flood Plain Deposits (a₁)

Alluvium flood plain deposits of the Tauranga Group were encountered underlying the topsoil to the target depth within boreholes AH3 AH6 and AH8. The soils here comprised predominately soft to very stiff clayey SILT / silty CLAY and in some rare instances layers of sandy SILT with some to minor fine to coarse gravels observed in AH6. Vane shear strengths within the soils measured ranging from 28kPa to greater than 198kPa.

7.3 Tauranga Group Alluvium - Terrace Deposits (a₂)

Alluvium terrace deposits of the Tauranga Group were encountered underlying the topsoil to the target depth within boreholes AH1, AH2, AH4, AH5 and AH7. The soils here comprised stiff to very stiff silty CLAY / clayey SILT, sandy SILT / silty SAND with some to minor fine to medium clasts. Vane shear strengths with the soils measured ranging 54kPa from to greater than 198kPa.



Alluvium terrace deposits is also inferred to be present below the topsoil in all CPT logs up to a maximum depth of 9.4m. The soil type classification output generally inferred similar material types to what was found within the nearby investigation points. The CPT sounding typically shows a resistance of less than 2MPa to 12MPa.

7.4 Tauranga Group Alluvium - Dissected Terrace Remnants (a₃)

The Cone resistance plots of the CPTs indicate a sudden increase in cone resistance after 9.4m likely as a result of encountering densely compacted alluvium materials. The soil behaviour type classification of CPT generally inferred these materials being 'sandy SILT / silty SAND' and clean SAND. Here theses deposits have been interpreted as dissected terrace deposits of the Tauranga Group.

7.5 Scala Penetrometer testing

The scala penetrometer testing encountered effective refusal in boreholes AH5 and AH6 between 3.2m and 5.0 meters below ground level (mbgl). Effective refusal was not encountered within the rest of the hand auger boreholes. Interpretation of these results suggests that dense soils are likely at variable depths across the site.

Hole ID	Topsoil (m)	a₁ (m)	a ₂ (m) a ₃ (m)		Scala Penetrometer Depth Range (m)	
AH1	0.0 – 0.2	n/a	0.2 – 5.0*		5.0 - 6.9 ∆	
AH2	0.0 - 0.2	n/a	0.2 – 4.5*		4.5 - 5.9 ∆	
AH3	0.0 – 0.3	0.3 – 3.5*	n/a		3.5 - 5.95 ∆	
AH4	0.0 - 0.2	n/a	0.2 - 3.85*		3.85 - 6.30 ∆	
AH5	0.0 – 0.3	n/a	0.3 – 3.55*		3.55 – 5.0	
AH6	0.0 - 0.2	0.2 -2.0*	n/a		2.0 - 3.2	
AH7	0.0 – 0.2	n/a	0.2 – 2.6*		2.6 - 4.6 ∆	
AH8	0.0 - 0.2	0.2 – 5.0*	n/a		5.0 - 6.9 ∆	
CPT1	0.0 - 0.3	n/a	0.3 – 7.1	7.1 – 20.0*	n/a	
CPT2	0.0 – 0.3	n/a	0.3 – 9.4	9.4 – 20.0*	n/a	

Table 1Summary of Subsurface Information

Note, all depths indicated are in mbgl

n/a - not applicable

 Δ = Scala penetrometer refusal not encountered

^{* =} Terminated depth of borehole/testing



7.6 Groundwater

Groundwater levels were measured in all boreholes at the time of drilling and on a return trip on the 19 February 2019. Groundwater was found to be present in all boreholes, excluding AH7 and CPT1, at depths of between 1.65m and 3.8mbgl. An indication of the groundwater levels is represented in Table 2. Groundwater levels do fluctuate and it must be appreciated that higher groundwater levels may be encountered following periods of prolonged or heavy rainfall.

Hole ID	Groundwater Levels (mbgl)			
	Day of Drilling 14-18/02/2019	Remeasured 19/02/2019		
AH1	2.3	2.93		
AH2	2.0	2.5		
AH3	1.45	1.65		
AH4	2.5	2.61		
AH5	3.1	3.1		
AH6	1.1	1.3		
AH7	2.0	Dry		
AH8	1.3	2.52		
CPT1	5.7	Hole collapsed		
CPT2	5.8	3.8		

Table 2Groundwater measurements

8. SITE CLASSIFICATIONS

8.1 Expansive Soils

Based on experience of similar soils elsewhere, the near surface clayey silt materials of the Tauranga Group alluvium, as noted in the boreholes, are susceptible to swelling and shrinking under seasonal variations of water content. For the purposes preliminary of design, the proposed development area may be designated as moderately reactive (Class M) in accordance with AS2870:2011. Shrink swell testing should be carried out once site formation works are complete to confirm the shrink swell class.



8.2 Site Subsoil Class

From findings in the boreholes, the subsurface comprise alluvial deposits for more than 5m and material with undrained shear strength of greater than 12.5kPa. Therefore, the site may be classified as subsoil Class C – Shallow Soil Site, in accordance with NZS 1170.5:2004, Section 3.1.3.

9. GEOTECHNICAL DESIGN PARAMETERS

Geotechnical design parameters for the main geological materials have been assessed using measured in situ shear vane strengths and based on our experience of similar soils across the Auckland area.

The parameters adopted for use in our stability analysis are provided in Table 4 below:

Stratum	Bulk Unit Weight	Effective Stress Parameters		
	(kN/m³)	Cohesion c' (kPa)	Angle of Friction, \mathscr{Q}'	
Colluvium	18	2	20	
Alluvium Floodplain Deposits (a₁)	18	3	28	
Alluvium Terrace 18 Deposits (a₂)		5	30	

Table 4: Geotechnical Parameters used in stability analyses

10. SLOPE STABILITY

As indicated in Section 2 and 4 of this report, slopes on the north and northeast edges of the knoll are moderately to steeply sloping, with surficial surface movement observed over this area.

To assess the stability of the northern knoll slope, a representative cross section (A - A') was selected for computer analysis based on the topographical information from survey plans from Lands and Survry (Appendix A). The location of the cross section is shown on the Site Plan, attached as Sheet 1. Details of the analyses are contained in the Appendix C. The analyses were undertaken using the computer based program "SLIDE" Version 6.039 by Rocscience.



The analyses, were undertaken based on the following load cases:

- 1. Static case measured groundwater conditions,
- 2. Static case raised groundwater conditions (modelled to reflect a possible raised groundwater following a period of prolonged, intense rainfall), and,
- 3. A seismic scenario, modelled using measured groundwater conditions with a seismic horizontal acceleration coefficient of 0.12g, (based on a 150yr earthquake return period as per NZS1170.5:2004).

For all scenarios modelled we have assessed potential circular surfaces using the Spencer method. The geotechnical parameters used in the analyses are summarised in Table 3 of Section 9.

A summary of the Factor of Safety results from the analyses are presented in Table 4 below. Output of the slope analyses is enclosed in Appendix C.

Cross Section	Factor of Safety			
	Measured Groundwater	Raised Groundwater	Seismic	
A - A'	2.1 🔨	2.1 🔨	1.7 🔨	
Accepted by Council	1.5	1.3	1.2	

Table 5: Factor of Safety obtained in Stability Analysis

X = unsatisfactory result, \checkmark = satisfactory result

We have carried out slope stability for the proposed subdivision on the current topographic profile. It is our professional opinion that slope stability of the current ground profile is not a concern for the site provided the recommendations in Sections 12 are followed.

11. LIQUEFACTION ASSESSMENT

To address the potential of liquefaction at the site, the CPT results were analysed using CPT liquefaction software 'Cliq', by Geologismiki Geotechnical Software. The software includes normalisation of the data for overburden pressure and is considered to provide indications of liquefaction potential. We point out that the CPT sounding was advanced to a depth of 20.7m and hence liquefaction analysis does not account for any susceptible layers below this depth.



The liquefaction analyses were completed for both Serviceability Limit State (SLS) and Ultimate Limit State (ULS) design criteria, using CPT results. Calculations were performed over the full depth of investigation. This section presents the potential of liquefaction in terms of Factor of Safety (FoS) used to assess the liquefaction vulnerability of the site.

The triggering of liquefaction was assessed using Boulanger and Idriss (2014) procedure as suggested in NZGS Earthquake Geotechnical Engineering Practice 'Module 3: Identification and Assessment of Liquefaction Hazards'. The following design parameters are used for the determination of Peak Ground Acceleration (a_{max}):

Table 5: Peak Ground Acceleration design parameters

Design Life (years)	Importance Level	ULS Return Period	SLS Return Period	Seismic Site Class	Magnitude M _w	Site Response Factor, f	C _{0,1000}
50	2	1/500	1/25	С	6.0	1.33	0.15g

For estimating the liquefaction potential at the site, the NZGS Module 1 Section 5.1 is referred in calculating the corresponding design peak ground acceleration (a_{max}) . The following a_{max} were adopted in the assessment.

- a_{max} for ULS is 0.15g, M_w is 6.0
- a_{max} for SLS is 0.04g, M_w is 6.0

Under ULS conditions several layers within the upper 20m returned FoS readings of 1 or below within logs CPT1 and CPT2. The estimated accumulative settlement, based on CPT1, is less than 35mm and lateral displacement is less than 350mm. The estimated accumulative settlement, based on CPT2, is less than 40mm and lateral displacement is less than 500mm. For both CPTs, no liquefaction is expected under SLS conditions. Therefore, the liquefaction potential of the Tauranga Group Alluviums at the site is negligible under SLS and low under ULS conditions. Furthermore, liquefaction in the top 10m occurs in layers of limited thickness (approximately less than 10%) and results in relatively small lateral displacements and vertical settlements. The results of the Cliq analyses are appended as Appendix D.



12. PRELIMINARY DEVELOPMENT RECOMMENDATIONS

The preliminary recommendations provided below assume that the building typically comprises a NZS3604:2011, lightweight type structure and that minor platform formation earthworks will be undertaken. It is our professional opinion that the building platform area shall remain safe and stable following development, provided that the recommendations below are adhered to.

12.1 Site Formation Works

At the time of preparing this report, the extent of the earthworks and detailed design drawings were not available. As such, we consider that it will be necessary to review future drawings to confirm the recommendations made in this report.

The site formation works are expected to be limited to a topsoil strip for the formation of the building platforms and vehicular accessway. Care must be taken during the topsoil strip to identify any buried features or soft ground. Any unsuitable material excavated as part of the formation works should be disposed of accordingly off site.

Any potential excavations into natural ground (up to 0.5m vertical height) are expected to be temporarily stable, provided they are left unsupported for the shortest possible duration. If they are to be left unsupported during prolonged wet weather, appropriate temporary support measures must be put in place. Work must be undertaken to ensure that surface water is not allowed to pond and infiltrate the ground surface on or immediately above any excavated face. Where any excavations greater than 0.5m are proposed, geotechnical input will be required at the Building Consent stage.

With potentially expansive sites, it is very important that the soils at slab subgrade are not permitted to dry out as they will re-swell on wetting (in the months after pouring the slab), exerting significant swelling pressures and potentially causing damage to the floor slab. We therefore recommend that the prepared pad be promptly covered with at least 100mm of GAP20 type material or similar and that the area is periodically wet down for at least one week prior to slab placement. Similarly, it is essential that footing trenches are not permitted to become desiccated over time, and these should be protected with at least 50mm of site concrete within 1 day of excavation. These measures will reduce the risk of 'hogging' and cracking of the slab. Cracking cannot be totally eliminated and it must be recognised that most concrete slabs can and do crack for many different reasons.



12.2 Preliminary Foundation Recommendations

The foundation requirements at the site are subject to the building materials, heavy loads, earthworks and location within the proposed subdivision. Provided the proposed structures are located at least 4.5m away from the crest of slopes with a gradient 1:3 or steeper, we consider that NZ3604:2011 type structures are appropriate for the development on each Lot.

The building platform should be located on ground cleared of any topsoil and soft soils. Fill up to 0.5m may be suitable for the site and should comprise compacted GAP40 aggregate. Where fill greater than 0.5m is proposed, further geotechnical input will be required

For shallow foundations, the natural in situ soils are able to provide an unfactored ultimate bearing capacity of 300kPa.

If any of the proposed developments are located within 4.5m of the crest of slopes with a gradient 1:3 or steeper or comprises heavy construction materials, specific engineering investigation design is required.

Irrespective of the above, the detailed development drawings for the new subdivision should be submitted to a suitably qualified engineer for review to confirm requirements at Building Consent stage.

13. ACCESSWAY

Based on our experience of similar subgrade soils and testing taken across the proposed accessway, a design CBR value of 3% would be appropriate for the underlying in situ subgrade soils located above elevations of 4.4m. Areas located below an elevation of 4.4m, a CBR value of 1% should be adopted.

During scala penetrometer testing a stiff crust was observed across the low lying areas (Elevation of less than 4.4m) to a depth of approximately 0.5mbgl. We suggest that any excavations across these areas are limited to avoid exposing any soft material. A geogrid, such as a Tensor TriAx geogrid, should also be placed between the natural soil and fill to provide additional support in these low lying areas.



14. STORMWATER

Stormwater from dwellings and all hard standing area must be collected and discharged in a manner in accordance with current Council requirements. To ensure that stormwater does not adversely affect site stability, it is important that all stormwater runoff from roof, deck, driveway and other sealed areas, together with discharges from perforated draincoils behind retaining walls, is collected by means of sealed pipes or swale and discharged accordingly offsite in a controlled manner. Under no circumstances is stormwater allowed to discharge directly onto the steep slopes below the building platforms or into soakpits.

15. DRAWING REVIEW

This report has been prepared specifically for the development proposal stated within Section 3 of this report as part of a Resource Consent application. We recommend that, when Building Consent drawings become available, we are allowed to review the drawings to ensure that the preliminary recommendations of this report remain valid. Additional Lot specific investigation boreholes may need to be drilled and further analyses may be required to ensure that the proposed formation works will not negatively impact slope stability.

16. LIMITATIONS

The conclusions made in this report are based upon the results of hand auger holes and CPTs spaced about the site as appeared appropriate at the time the field exploration was carried out. We also point out that the holes were extended as deep as reasonably possible with hand operated equipment but they could not and did not penetrate into the underlying slightly weathered materials. We are therefore not able to report on the potential of any deep-seated bedding plane defect or other adverse lithological feature in the underlying parent rock.

The report was prepared in the context defined in Section 1 above and must not be relied upon by any other party other than that for whom it was prepared and the relevant Territorial Authority. It has been compiled with respect to the brief given to us, and must not be relied upon in any other context or recreated for any other purpose.



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APPENDIX A

Draft Concept Plans and Survey Drawings (Greenwood Associates &

Lands and Survey)

greenwoodassociates | Landscape Architecture

Landscape Plan Set for

Stratford Properties

278 Clevedon-Kawakawa Road Clevedon, Auckland

912/1 - Masterplan with Aerial 912/1 - Topographical Plan

14/01/19 14/01/19



greenwoodassociates.co.nz

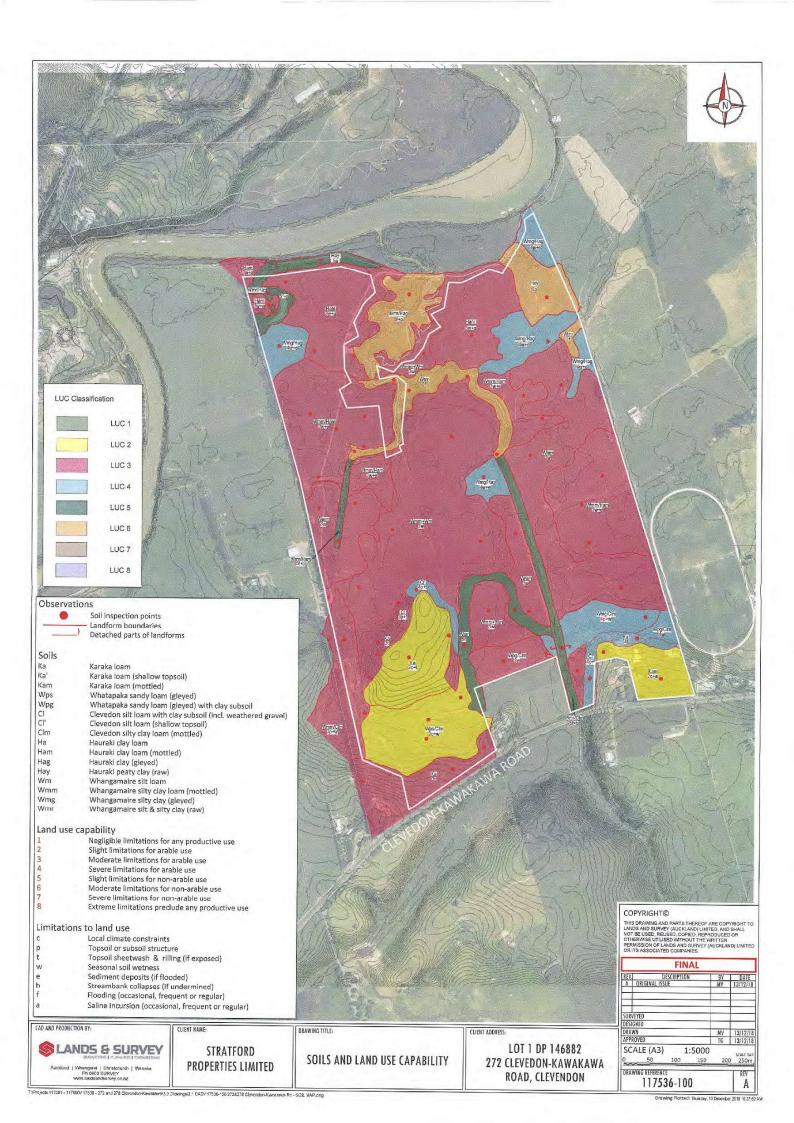


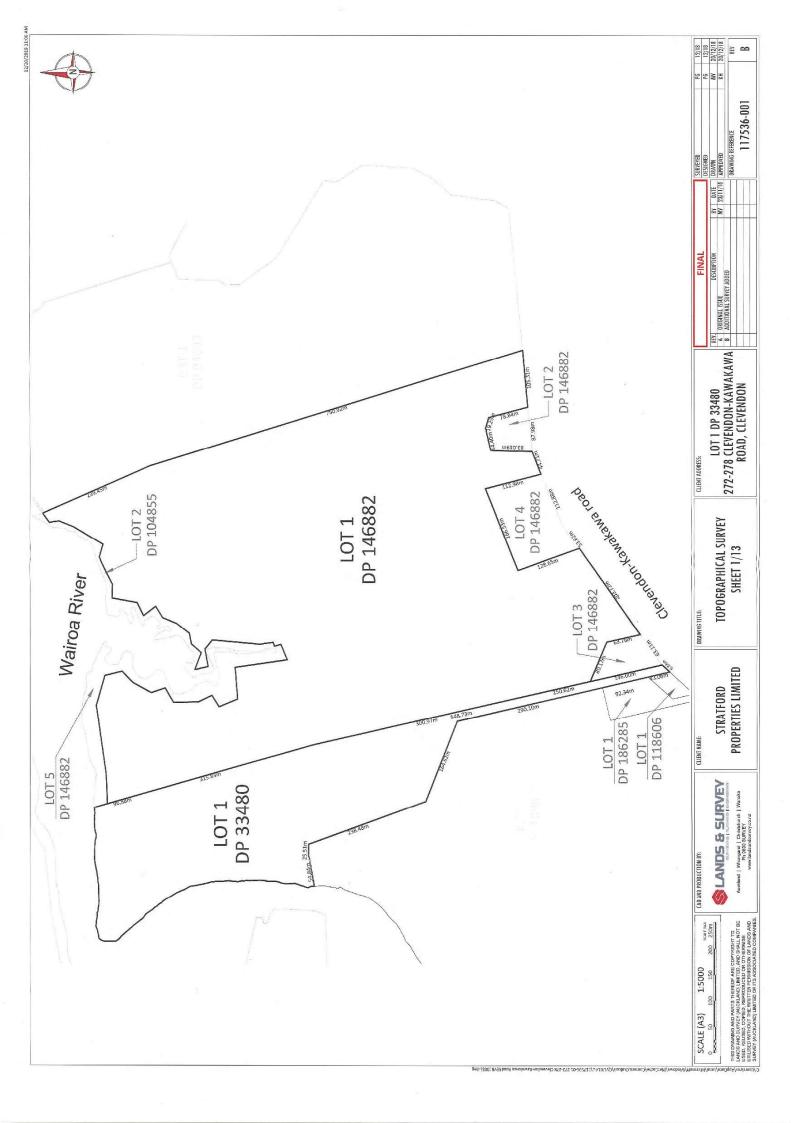


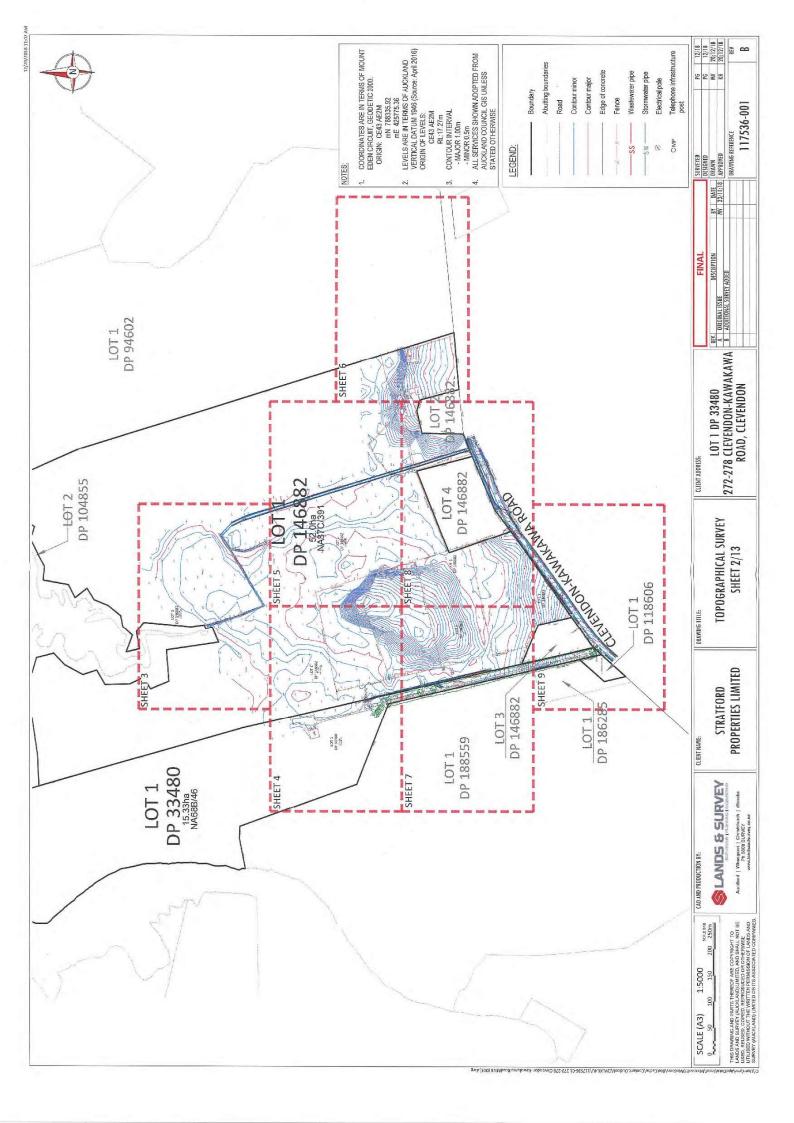


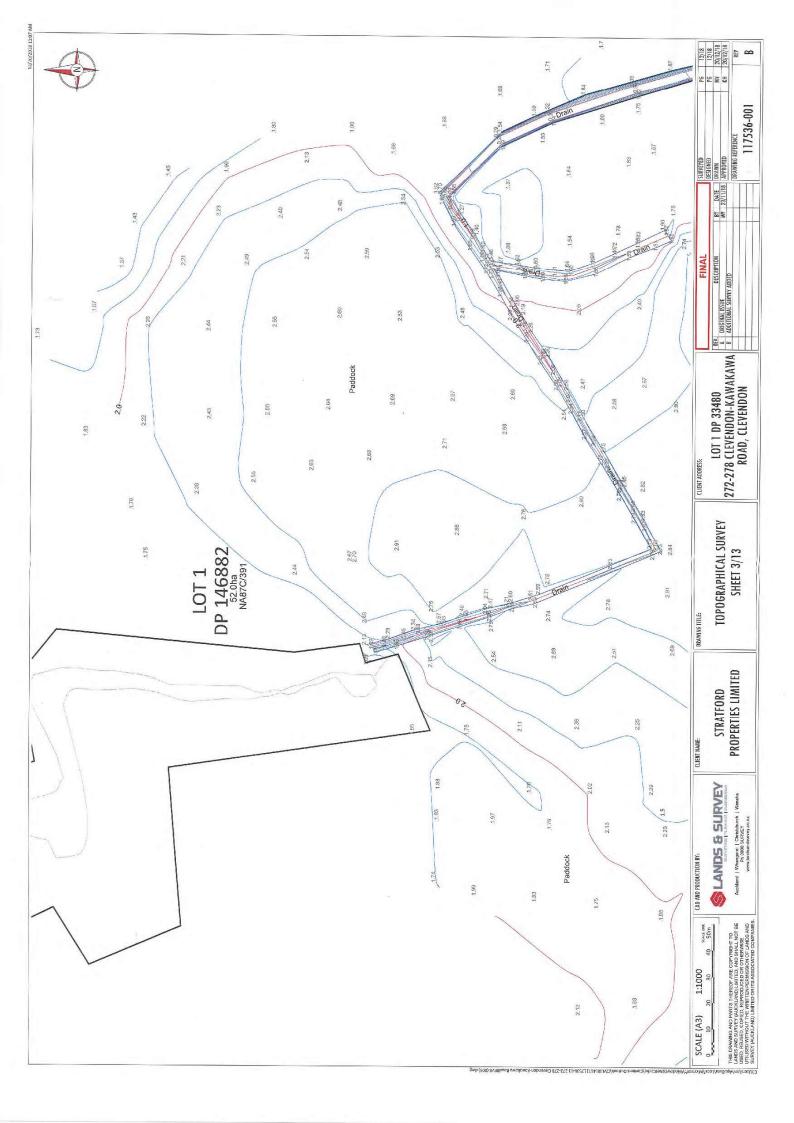


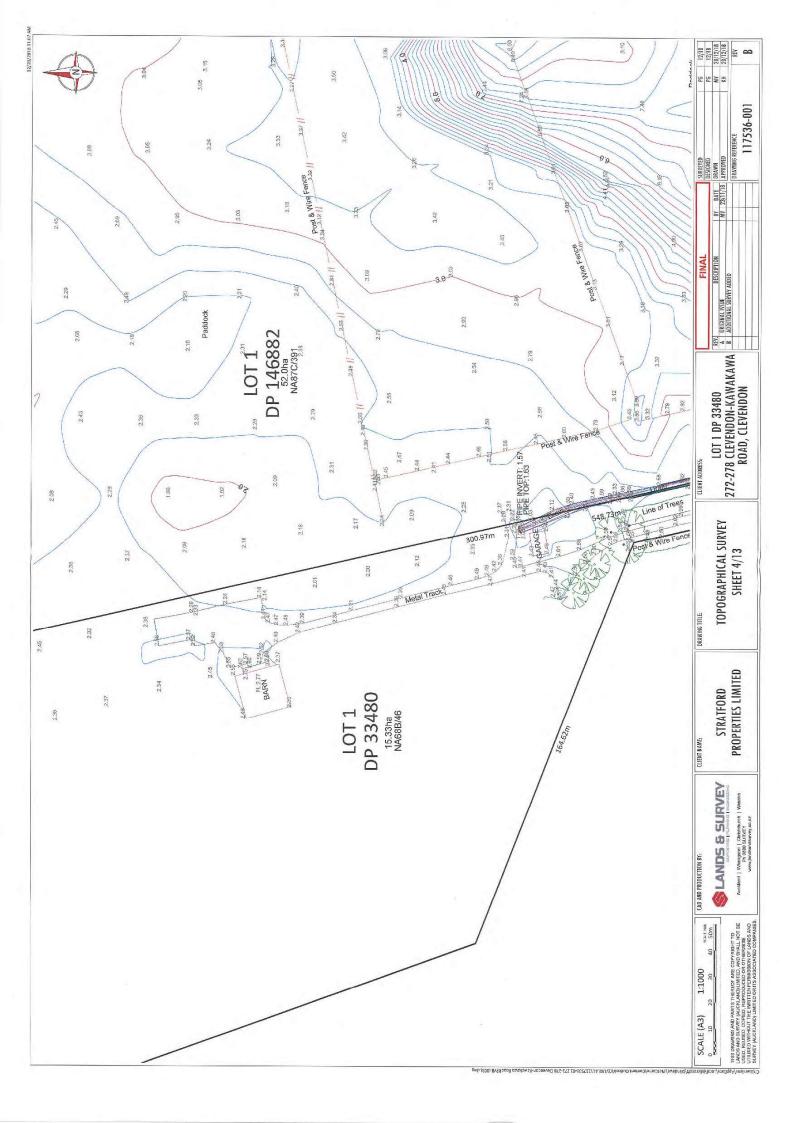
greenwood associates Landscape Architecture

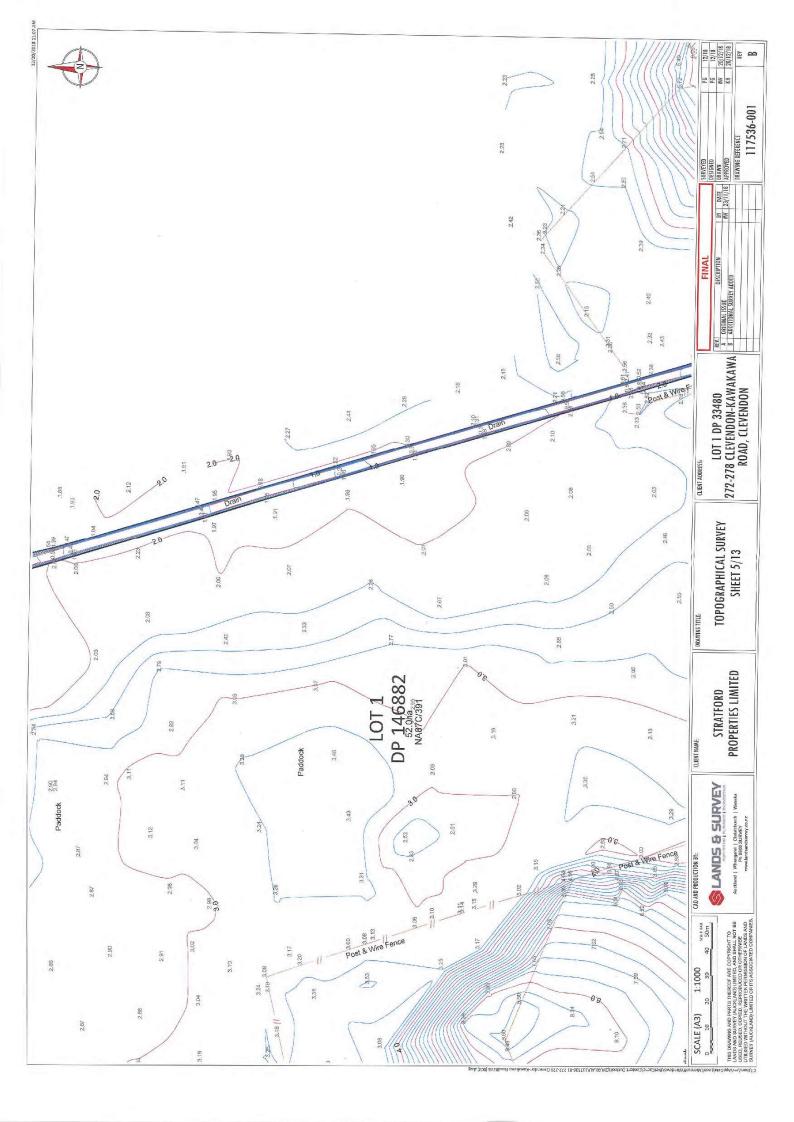


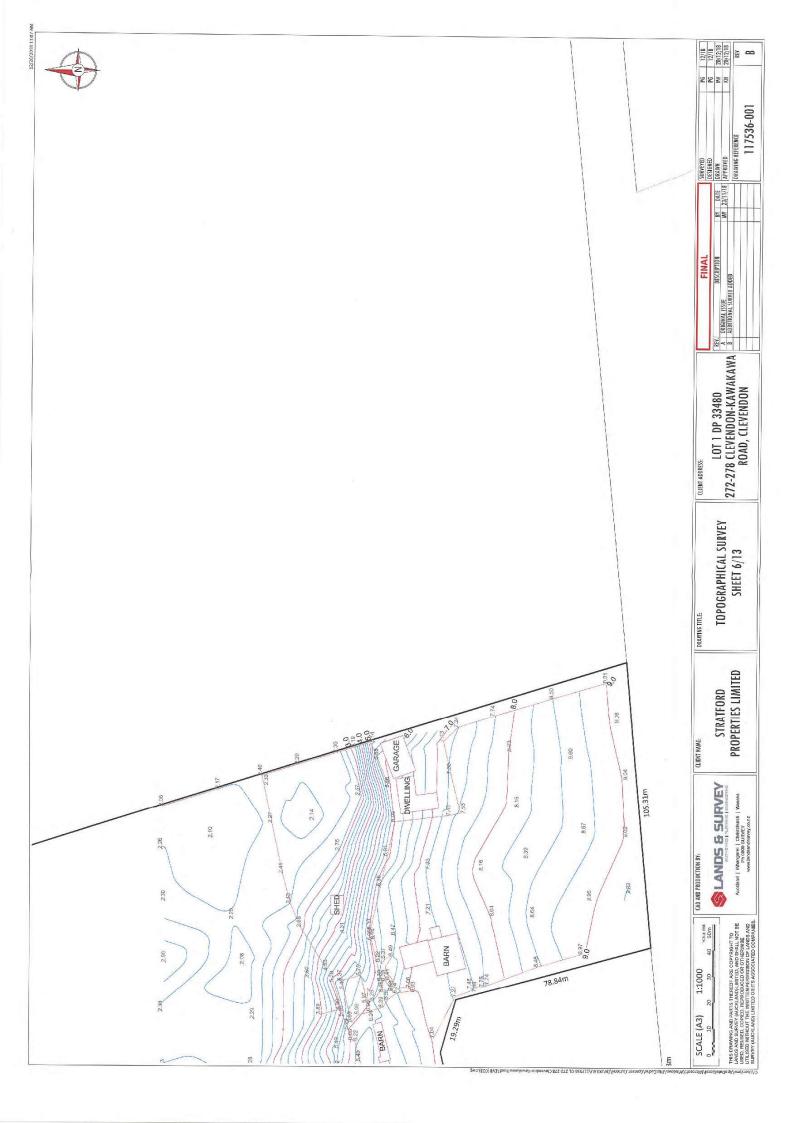


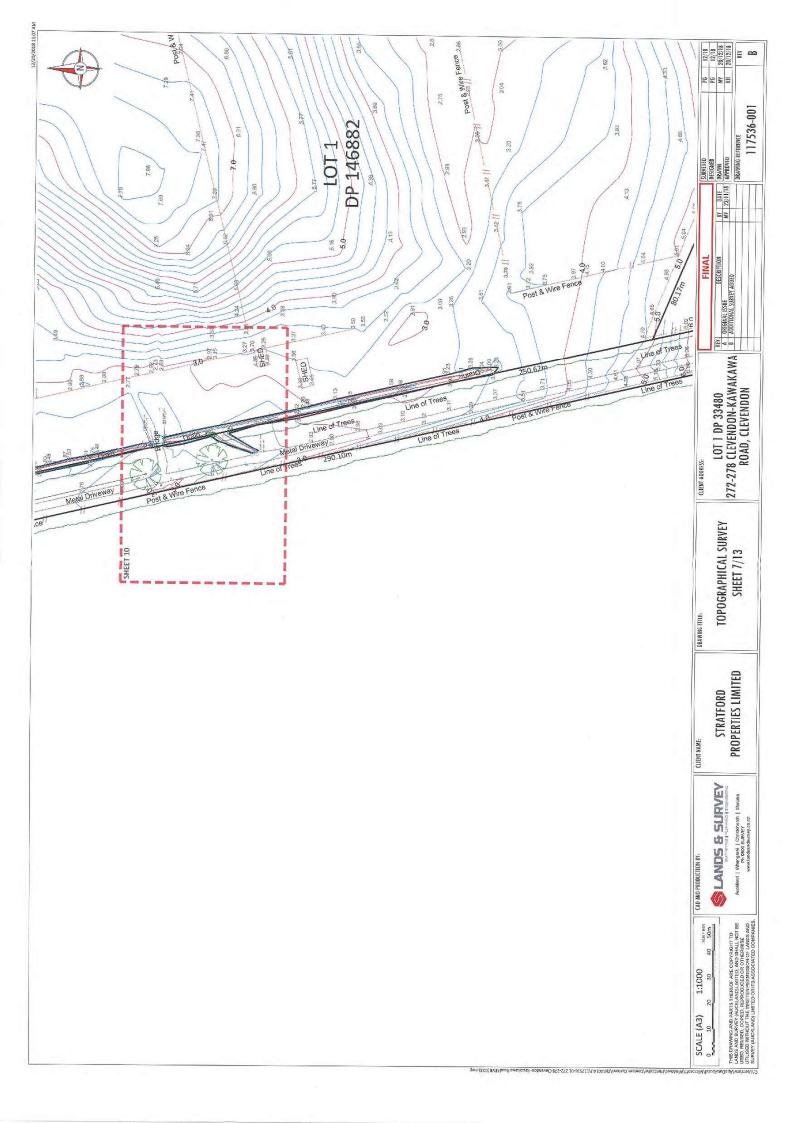


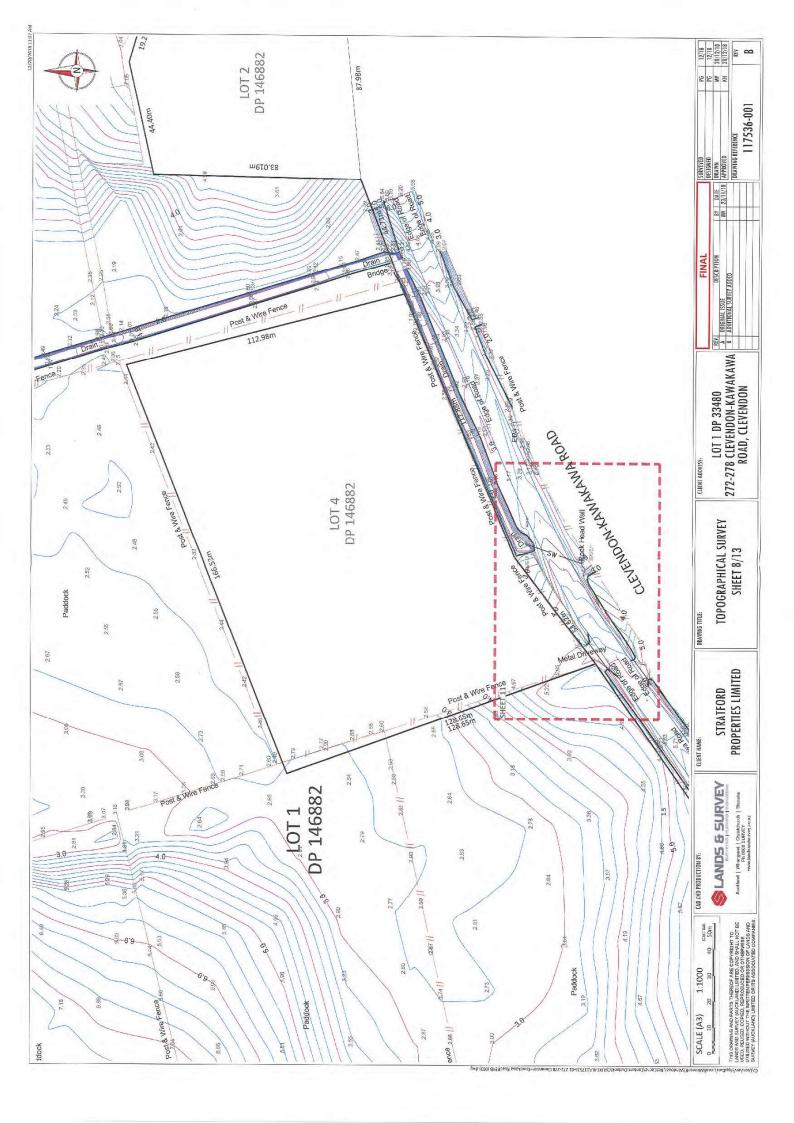


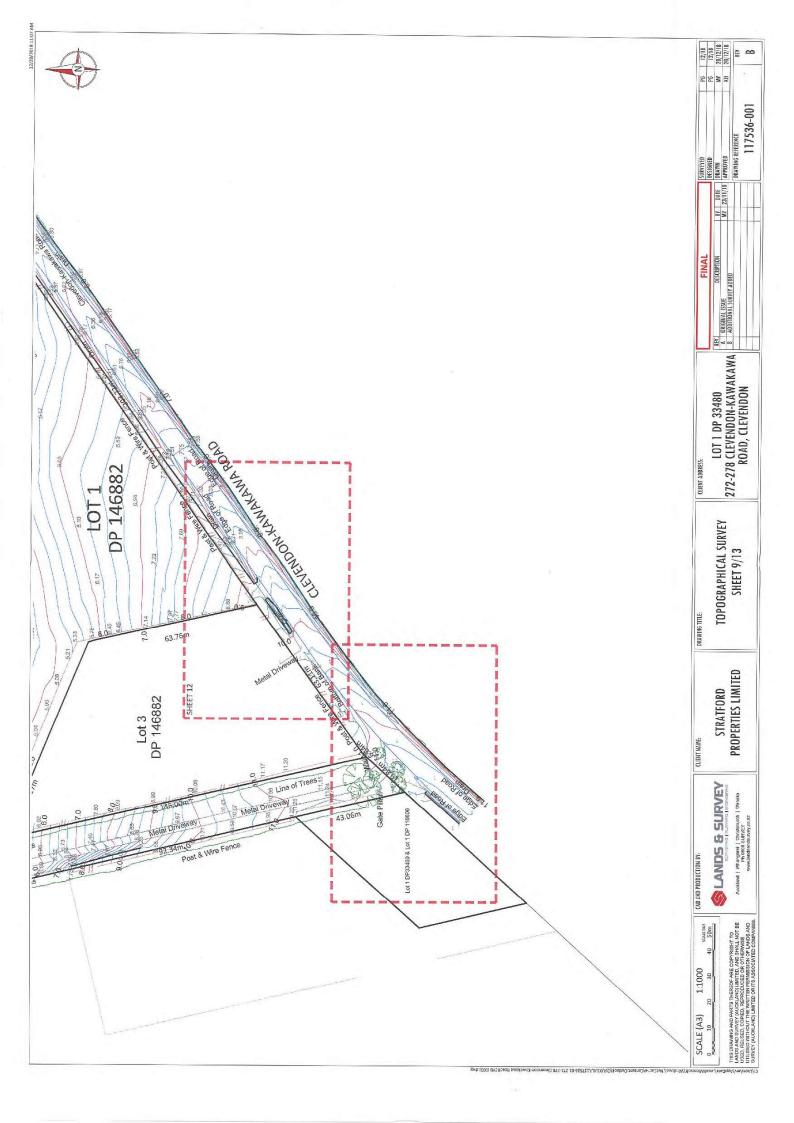


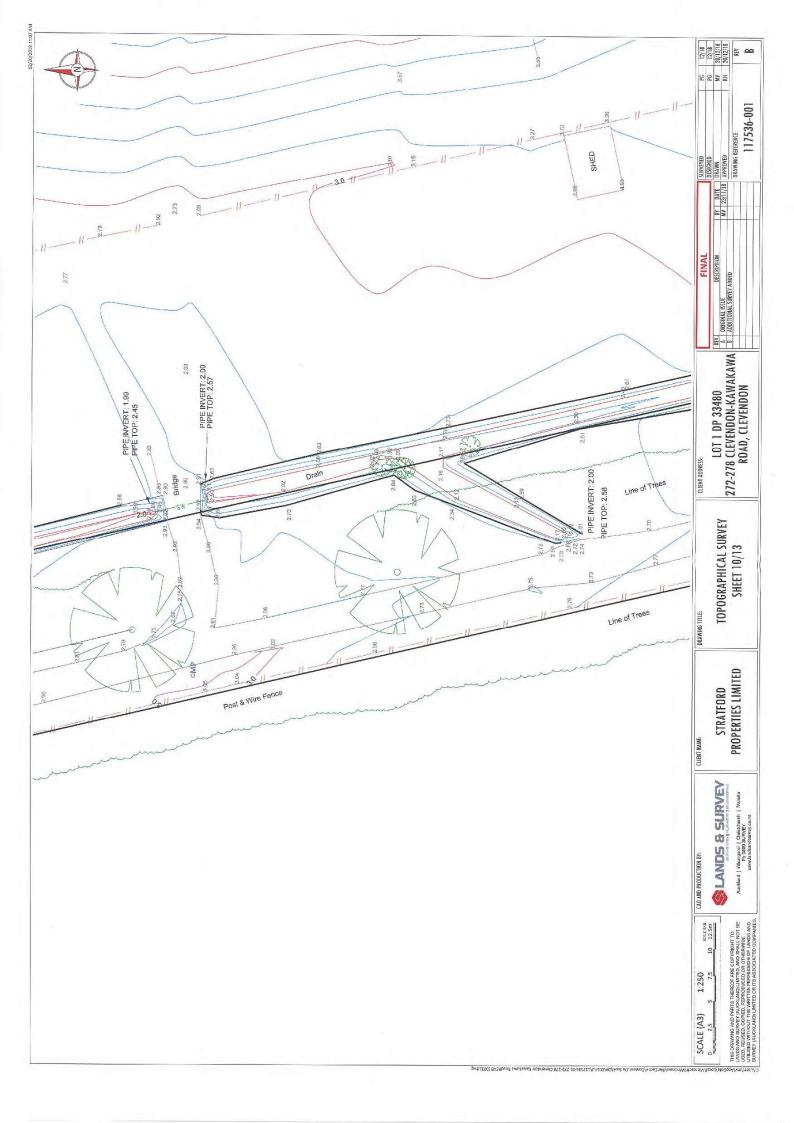


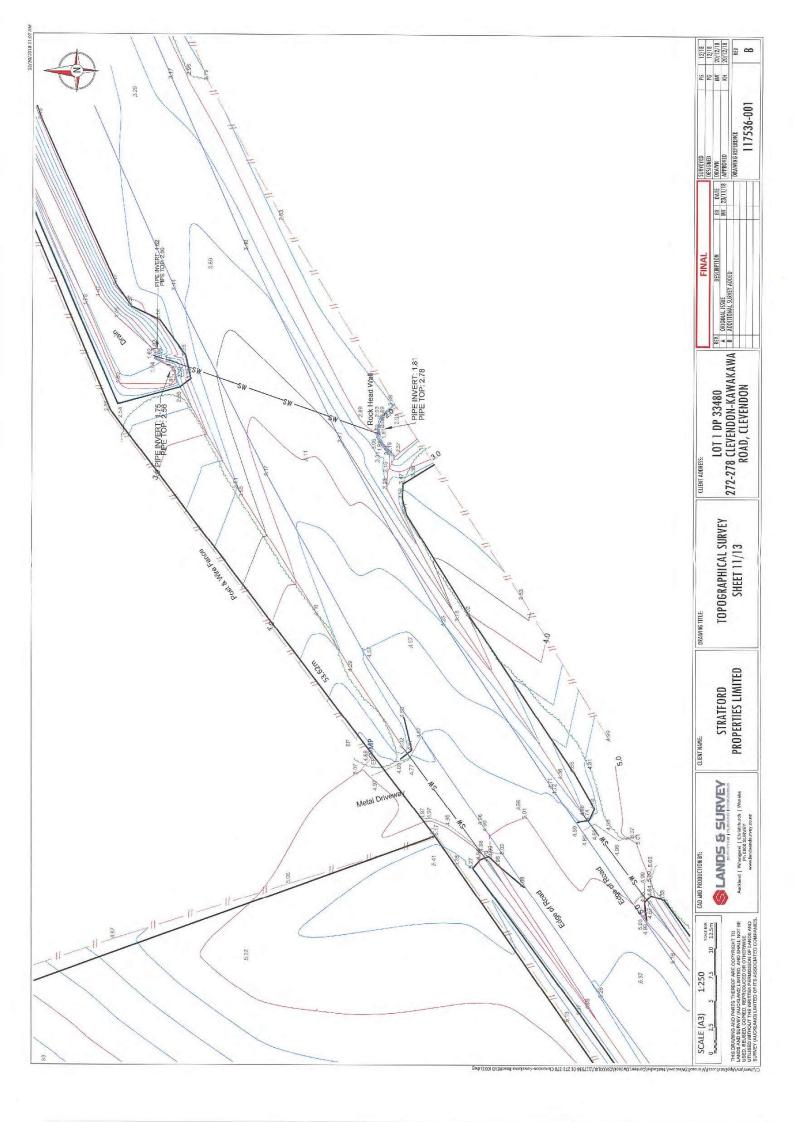


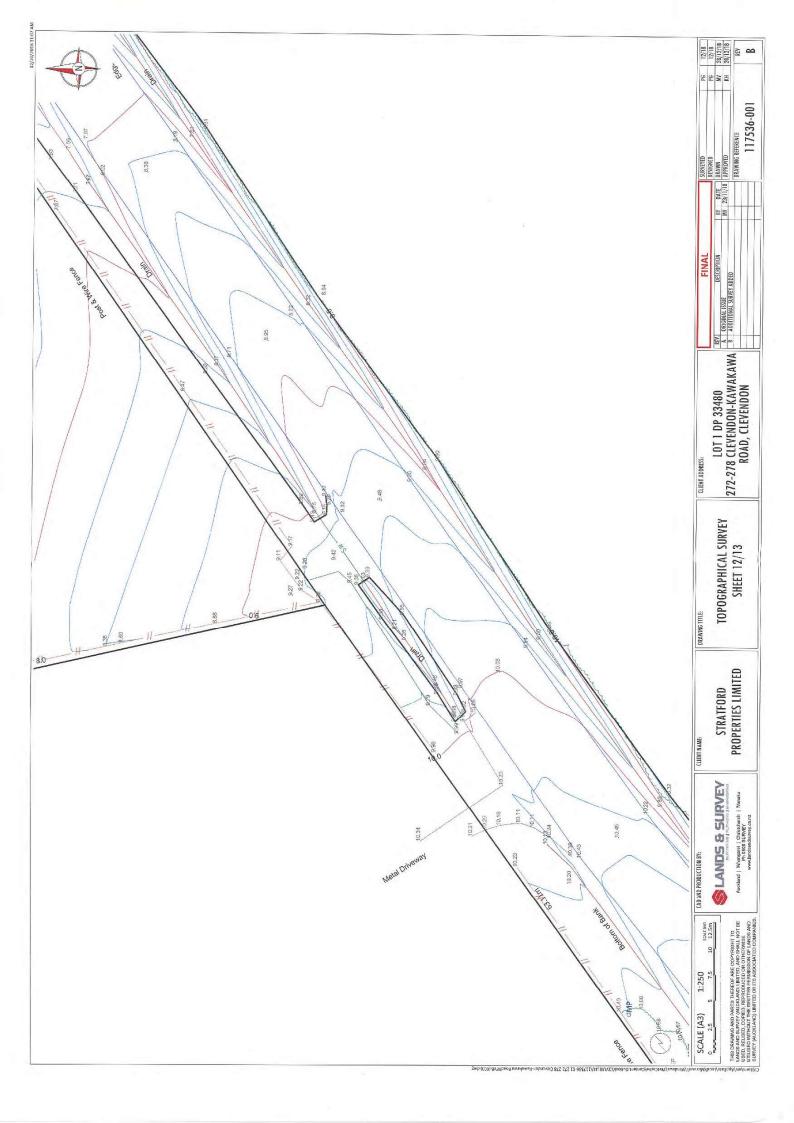


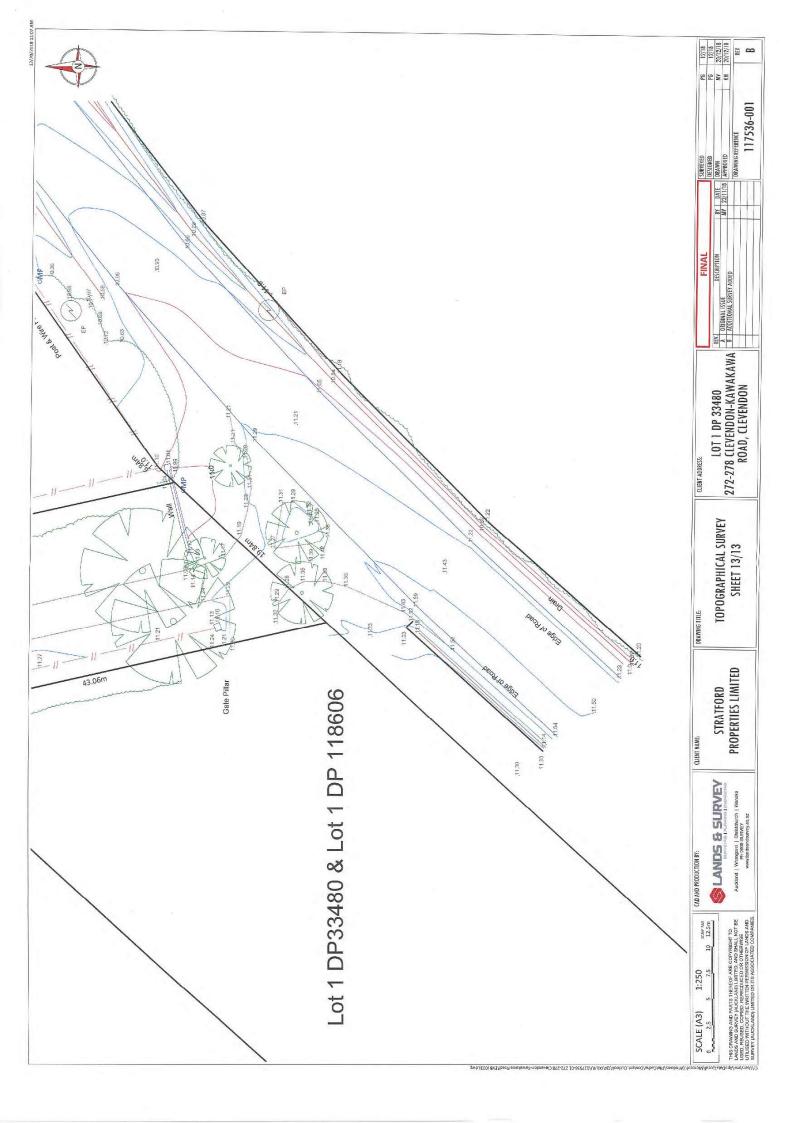














APPENDIX B

Subsurface Investigation Logs

HAND AUGER LOG									Job No.: 190051			051
Clie	nt:	KGA Geotechnical Group Ltd							Hole	No.:	Α	-11
Proj	ect:	272-278 Clevedon-Kawakawa Road, Cleve	edon						Date:		15/02	/2019
Loca	ation:	See Site Plan							Logge	ed By:	S	R
Coo	rdinat	es: ,		Gro	ound L	evel: -			Sheet	t:	1 0	f 1
Depth (m)	RL	Subsurface Conditions	Groundwater	Geological Unit	Graphic Log			(kPa	Streng) or details		Penetr (blows	ala ometer / 50mm)
			טֿ	G	ษ	50	100	150	200	Values	Depth (m)	Blows
_		Topsoil. [TOPSOIL]		TOP	<u>مه</u> ۲۵ مه						5.05	1
_		SILT with some clay. Orange mottled light grey, very	1	⊢σ	₩ <u>×_</u> ×		Ì				5.10 5.15	1 1
_		stiff to hard, dry, low plasticity. [ALLUVIUM] Clayey SILT. Orange mottled light grey, very stiff to	1		<u>نه به</u> مر <u>ب</u> به م		1	-		198+	5.20	1
0.5		hard, dry, moderately plastic. [ALLUVIUM]			× × × ×			-		-	5.25 5.30	1
_		Silty CLAY. Orange mottled light grey, very stiff to	-		<u>× ×</u>						5.35	1
_		hard, dry to moist, highly plastic.			×		1	1	 		5.40	1
1.0-		At 1m; Becomes very stiff, moist and light grey			×		1			139	5.45 5.50	1 2
- 1.0		mottled orange. [ALLUVIUM]			* *				1	57	5.50 5.55	2
-					×			ł			5.60	2
-					* *			Ì	1		5.65	1
1.5-					×		i	L İ		124	5.70	2
_		1.6m: Moist to wet.		its)	× ×			i i		59	5.75 5.80	2 2
-		Tom. Moist to wet.		sod	× _						5.85	1
				e de	×			÷			5.90	2
2.0-		1.9m: Becomes orange and light grey. CLAY with some Silt. Orange mottled light grey, very	-	Sene	¥ -		1	■ ¦		141	5.95	2
_		stiff, moist to wet, highly plastic. [ALLUVIUM]		stoc						74	6.00	2 2
			Z š	Plei					1		6.05 6.10	2 3
_			5/02/2019	Σ							6.15	2
2.5-		Silty CLAY. Light grey mottled orange, stiff, moist to		OUP ALLUVIUM (Pleistocene deposits)	x				1	99 48	6.20	3
		wet, highly plastic. [ALLUVIUM]			×			Ì		40	6.25	2
			J2/2019	ΡA	× ×		į	į			6.30 6.35	2 2
_			22/2		*		- i	i.			6.40	3
3.0-		3m: Becomes wet, very stiff with occasional	19/0	GR	×			∎ į		127 48	6.45	2
		organics (<2mm).		IGA	× ×					+0	6.50	2
_				RAN	* <u>*</u>						6.55 6.60	2 2
_				TAURANGA	× ×					99	6.65	2.5
3.5		Clayey SILT with minor fine sand. Orange mottled			<u> × ×</u> ×	222;	ļ	÷		42	6.70	2.5
_		light grey and dark orange, stiff, wet, moderately plastic. [ALLUVIUM]			× × ×						6.75	2.5
-						1		÷			6.80 6.85	2.5 2.5
4.0-			_		× × ×					116	6.90	2.5
		Silty CLAY with some fine to medium sand. Orange mottled light grey and dark orange, very stiff, wet,			× ×	<u></u>	į			57		
-		highly plastic. [ALLUVIUM]			×							
					× ×				 			
4.5					× ×					127		
-					× ×		1			45		
					× .							
					× × ×					60		
5.0		5m: End of Borehole	-							62 20		
							i	i	i 			
		bbreviations										
Soils	logged	in accordance with 'The guidelines for the classification a	nd des	cription	n of soil a	and						

rock for engineering purposes' December 2005, NZGS

Produced with Core-GS

SOIL DYNE LTD AUCKLAND **Other Comments** Water Shear Vane Corrected as per NZGS Guidelines Vane No.:GEO1596 is 1.414 ▼ Standing Water Level Flat, Field. Hole data is for a set M: 027 368 8832 location only. UTP = Unable To Penetrate \bigtriangledown Water Level At Time Of Drilling Soil Dyne Ltd + = Peak Exceeded E: soil.dyne@yahoo.com - = No Result

		HAND AUGER	LO	G				Job	No.:	190	051	
Clie	nt:	KGA Geotechnical Group Ltd						Hole No.:		AH2		
Proj	ect:	272-278 Clevedon-Kawakawa Road, Cleve	don					Date		15/02	2/2019	
Loca	ation:	See Site Plan						Logg	ed By:	S	R	
Coo	rdinat	es: ,		Gre	ound L	.evel: -			Sheet: 1 of 1			
			ŗ		6					50	ala	
Depth (m)	RL	Subsurface Conditions	Groundwater	Geological Unit	Graphic Log		ne Shea (kF efer notes	Pa) for detail	s)	Penetr	ometer / 50mm)	
					-	50	100 15	0 200	Values	(m)	Blows	
_		Topsoil. [TOPSOIL]		- sol	≗TS ⊴ ⊛					3.05 3.10	1	
		Clayey SILT. Orange, very stiff, dry, low to			<u></u>			I I I		3.15	1	
_		moderately plastic. [WAIPAPA GROUP /			× × ×			1		3.20	1	
0.5					× <u>+</u> + <u>-</u> ×-	77		i I	141	3.25	1	
_		Silty CLAY. Orange mottled light grey, very stiff, dry						1	28	3.30	1	
_		to moist, moderate to highly plastic. [WAIPAPA GROUP / COLLUVIUM ?]			×					3.35	0.5	
-					× ×		i i	i I		3.40	0.5	
-		0,9m: Becomes moist.			×	-			184	3.45	1	
1.0		o.om. Decomes moist.			×	////			62	3.50	2	
-					× ×			i I	02	3.55	1	
_		Clayey SILT. Orange mottled light grey, very stiff,	1		<u>× × ×</u>					3.60	2	
_		\ moist, moderately plastic. [WAIPAPA GROUP / /	1	sits	× × ×		i i			3.65	2	
1.5		COLLUVIUM ?]		ANGA GROUP ALLUVIUM (Pleistocene deposits)	* * * *	1		1	UTP	3.70	2	
1.5		SILT with minor to trace of clay. Light brown, mottled		de	×	i	1		- 1	3.75	2	
_		orange and light grey, very stiff, dry to moist, very		ene	* * *	i i	i i	i I		3.80	3	
_		low plasticity.		Ö	~ * ^ * ^			1		3.85	2	
_		At 1.5m; With a trace of clay, hard and orange mottled light brown, dark orange and light grey. At	019	eist	* * * *			1		3.90	3	
2.0		1.6m; With Clasts (<4mm<30%). At 1.7m; With some	¥ S	đ	× ×				UTP	3.95	2	
_		clay, [WAIPAPA GROUP / COLLUVIUM ?]	15/02/2019	Σ	6.0 6.0			1	-	4.00	3	
_		SILT with fine to medium, medium dense to dense		- F	· · · · · · ·			1		4.05	1.5	
_		Gravels, Clasts (<4mm) and fine to coarse Sand.	െ	Ċ		1		1		4.10	1.5	
_		Orange mottled orangey brown, moist to wet, no	▲ 9/02/2019	AL					UTP	4.15	1.5	
2.5		plasticity. [WAIPAPA GROUP / COLLUVIUM ?]	02/	4	°	1	1 1	1		4.20	1.5	
_		Fine to coarse, medium dense to dense SAND with	19	õ	· · ·			1	-	4.25	2	
		SILT, Fine to medium Gravels and Clasts (<5mm). Orangey brown and dark orange, saturated, no		ъ				1		4.30	2	
_		plasticity. At 2.4m; Becomes wet.		d B				1		4.35	2	
3.0-		At 2.6m; Becomes orange mottled light grey.	ļ	Å				1	Scaled	4.40	3	
		\[WAIPAPA GROUP / COLLUVIUM ?]		TAUR	* ** **			! !	-	4.45	6	
-		Fine to coarse, loose Sandy SILT with Clasts		TAL						4.50	6	
-		(<4mm) and minor clay. Orange mottled light grey,		`	*****					4.55	7	
-		wet, low plasticity. Scaled from 3m then re drilled. At 3.3m; Becomes light grey mottled orange and			×			1		4.60	6	
3.5		saturated. [WAIPAPA GROUP / COLLUVIUM ?]			× × ×					4.65	4	
-					** • *			1		4.70	4	
		3.7m: With Clasts (<5mm<30%).			N. X. X.			1		4.75	4	
					× * * *			I I		4.80	4	
4.0		Silty (Fine to coarse, loose) SAND with Clasts			× ×					4.85	5	
_		(<5mm) and minor clay. Light grey mottled orange,			×	i i	i i	i I		4.90	5	
_		saturated, low plasticity. At 4m; Medium dense. [WAIPAPA GROUP / COLLUVIUM ?]						1		4.95	5	
-					×			1		5.00	5	
-		Fine to coarse, medium dense Sandy SILT with	1		x x x			1		5.05	5	
4.5		Clasts (<5mm) and minor clay. Orange mottled light			X			1		5.10	6	
-		grey, wet to saturated, low plasticity [WAIPAPA								5.15	5	
-		GROUP / COLLUVIUM ?]						i I		5.20	6	
		4 Free Freed of Developing the second by the second s						1		5.25	5	
		4.5m: End of Borehole, unable to penetrate. Additional scala values. Start 5.5m;						1		5.30	6	
5.0		6,7,5,6,4,5,4,4,5.				1		1		5.35	6	
		Scaled 1m first re drilled, then scaled out 2m.								5.40	7	
		Then re drilled to 4.5m.				1		i I		5.45	7	
						1		I				

Soils logged in accordance with 'The guidelines for the classification and description of soil and rock for engineering purposes' December 2005, NZGS

Produced with Core-GS

	bols logged in accordance with the guidelines for the classification and description of soil and bock for engineering purposes' December 2005, NZGS							
Water	Shear Vane	Other Comments	AUCKLAND					
Standing Water ▼ Level	Corrected as per NZGS Guidelines Vane No.:GEO1596 is 1.414	Near Level, Field. Hole data is for a set location only.	M: 027 368 8832					
\bigtriangledown Water Level At Time Of Drilling	UTP = Unable To Penetrate + = Peak Exceeded - = No Result		E: soil.dyne@yahoo.com	S				



Client: KGA Geotechnical Group Ltd Hole No.: AH3 Project: 272-278 Clevedon-Kawakawa Road, Clevedon Date: 14/02/2019 Location: See Site Plan Ground Level: - Sheet: 1 of 1 Coordinates: . Ground Level: - Sheet: 1 of 1 Coordinates: Coordinates: . <t< th=""><th colspan="8">HAND AUGER LOG</th><th colspan="2">Job No.: 19</th><th>051</th></t<>	HAND AUGER LOG								Job No.: 19		051
Location: See Site Plan Logged By: SR Coordinates: Ground Level: Sheet: 1 of 1 Image: Subsurface Conditions Image: Sign of the status of t	Client:	:	KGA Geotechnical Group Ltd					H	ole No.:	Α	H3
Coordinates: Ground Level: Sheet: 1 of 1 Subsurface Conditions Image: Subsurface Conditions Image: Subsurface Conditions Scale Penetrometer (blows / 50mm) Image: Subsurface Conditions Image: Subsurface Conditions Image: Subsurface Conditions Scale Penetrometer (blows / 50mm) Image: Subsurface Conditions Subsurface Conditions Scale Penetrometer (blows / 50mm) Image: Subsurface Conditions Image: Subsurface Conditins Image: Subsurface Conditins <td< td=""><td>Project</td><td>:t:</td><td>272-278 Clevedon-Kawakawa Road, Cleve</td><td>don</td><td></td><td></td><td></td><td>Da</td><td>ate:</td><td>14/02</td><td>/2019</td></td<>	Project	:t:	272-278 Clevedon-Kawakawa Road, Cleve	don				Da	ate:	14/02	/2019
Coordinates: Ground Level: Sheet: 1 of 1 Image: Subsurface Conditions Scale Penetrometer (blows / 50mm) 0.5 Topsoil. (TOPSOIL) 50 100 150 200 Values (order notes for details) 0.6 3.65 0.5 3.65 0.5 3.65 0.5 3.65 0.5 3.65 0.5 3.65 0.5 3.65 0.5 3.65 0.5 3.65 0.5 3.65 0.5 3.65 0.5 3.85 0.5	Locatio	on:	See Site Plan					Lo	aged By:	S	R
Image: Subsurface Conditions Scale Penetrometer (blows / 50mm) 0.5 Topsoil. [TOPSOIL] 50 100 150 200 Values Depth Minimum Book 0.5 0.5 Clayey SILT. Grey motiled orange with brown staining, wery stiff, dry moderately plastic. [ALLUVIUM] Status 0.5 3.85 0.5 1.0 Silby CLAY. Orange and light grey, very stiff, dry to moderately plastic. [ALLUVIUM] 141 3.75 0.5 1.0 1.2m: Moist to wet. 1.2m: Moist to wet. 59 400 0.5 4.00 0.5 1.5 1.2m: Moist to wet. 1.7m: Becomes stiff with occasional plant fibers. 1.2m: Moist to wet. 59 4.20 1 144 4.50 1 2.6 2.5m: Becomes stiff with poor recovery and some contamination from above. 57 4.30 1 4.30 1 3.0 2.5m: End of Borehole, high suction 2.5m: End of Borehole, high suction 22 22 28 4.45 1 3.0 3.5m: End of Borehole, high suction 22 28 4.20 1 128 5.20 2			9 5 : ,		Gr	ound L	evel: -				
Topsoil. [TOPSOIL] Topsoil. [TOPSOIL] Topsoil. [TOPSOIL] Statistic (Comparison of the statistic of the				7						0	
Topsoil. [TOPSOIL] Topsoil. [TOPSOIL] Topsoil. [TOPSOIL] Statistic (Comparison of the statistic of the	epth (m)	RL	Subsurface Conditions	oundwate	eological Unit	aphic Lo	()	Pa)	-	Penetr (blows	ometer
0.5 Clayey SILT. Grey, motiled orange with brown staining, very stiff, dry, moderately plastic. 141 3,70 0.5 1.0 Sitty CLAY, Orange and light grey, very stiff, dry to most, high plastic. 3.80 0.5 1.0 1m: Becomes stiff with occasional plant fibers. 3.80 0.5 1.2m: Moist to wet. 4.15 1.5m: Wet. 4.16 3.40 1.5m: Wet. 1.5m: Wet. 4.16 1.41 4.30 2 2.0 Organic Silty CLAY, Dark brown, stiff, wet, moderate to highly plastic. 4.40 1 4.55 1 1.5m: Wet. 1.7m: Becomes grey. 4.40 1 4.55 1 2.0 Clayey SILT. Grey, firm, wet to saturated, moderately plastic. [ALLUVIUM] 14 4.55 1 3.0 3m: Fully saturated. 5m econtes stiff with poor recovery and some contamination from above. 5m econtamination from above. 5m econtamination from above. 5m econtamination from above. 3.5 3.5m: End of Borehole, high suction 22 22 22 22 5.15 3.5m: End of Borehole, high suction 22 5.30 2 5.30 2 3.5 3.5m: End of Borehole, hig				טֿ	G	ษ	50 100 1	50 20	0 Values		Blows
0.5 staining. very stiff, dry. moderately plastic. ALLUVIUM] 141 3.75 0.5 1.0 Sity CLAY, Orange and light grey, very stiff, dry to moist. highly plastic. At 0.6m; Moist. [ALLUVIUM] 3.85 0.5 1.0 1m: Becomes stiff with occasional plant fibers. 1.2m; Moist to wet. 99 3.95 0.5 1.6 1.5m; Wet. 4.06; Moist CLAY, Dark brown, stiff, wet, moderate to highly plastic. At 2m; Firm; (ALLUVIUM) 59 4.20 1 2.0 2.5m; Becomes grey. moderately plastic. [ALLUVIUM] 22 28 4.46; 1 2.0 2.5m; Becomes stiff with poor recovery and some contamination from above. 28 4.47; 1 3.0 3m; Fully saturated. 57 4.90; 1 4.86; 1 3.6 3.5m; End of Borehole, high suction 22 28 5.20; 2	-				TOPSO IL	⊵TS ⊴ ≝ere				3.60	0.5
1.0 Yes 3.173 0.5 1.0 Sitty CLAY. Orange and light grey, very stiff, dry to moist, highly plastic. At 0.6m; Moist, [ALLUVIUM] 3.4 3.473 0.5 1.0 1m: Becomes stiff with occasional plant fibers. 3.4 3.40 3.85 0.5 1.2m: Moist to wet. 1.2m: Moist to wet. 4.10 0.5 4.10 0.5 1.5m: Wet. 1.7m: Becomes grey. 4.15 1 4.15 1 2.0 Organic Silty CLAY. Dark brown, stiff, wet, moderate to highly plastic. At 2m; Firm. [ALLUVIUM] 2.8 4.45 1 2.5 2.5m: Becomes stiff with poor recovery and some contamination from above. 57 4.90 1 3.6 3.5m: End of Borehole, high suction 2.2 5.15 2 5.05 1 3.6 3.5m: End of Borehole, high suction 2.2 5.15 2 5.15 2 3.6 3.5m: End of Borehole, high suction 2.2 5.15 2 5.30 2 3.6 3.5m: End of Borehole, high suction 2.2 5.15 2 5.30 2 3.6 3.5m: End of Borehole, high suction 2.2 <t< td=""><td>-</td><td></td><td>Clayey SILT. Grey mottled orange with brown staining, very stiff, dry, moderately plastic.</td><td></td><td></td><td><u>× ×</u></td><td></td><td></td><td>141</td><td></td><td></td></t<>	-		Clayey SILT. Grey mottled orange with brown staining, very stiff, dry, moderately plastic.			<u>× ×</u>			141		
1.0 Shifty CLAY. Orange and light grey, very stift, dry to moist, highly plastic. At 0.6m; Moist [ALLUVIUM] 3.85 0.5 1.0 1m: Becomes stiff with occasional plant fibers. 1.2m: Moist to wet. 99 3.90 0.5 1.5 1.2m: Moist to wet. 415 1 1.0 415 1 1.5 1.5m: Wet. 59 4.20 1 4.15 1 2.0 Organic Silty CLAY. Dark brown, stiff, wet, moderate to highly plastic. At 2m; Firm, [ALLUVIUM] 59 4.22 14 4.50 1 2.6 2.5m: Becomes stiff with poor recovery and some contamination from above. 28 4.75 1 4.85 1 3.6 3.5m: End of Borehole, high suction 22 28 5.00 2 5.00 2 3.6 3.5m: End of Borehole, high suction 22 28 5.00 2 5.00 2 3.5m: End of Borehole, high suction 22 28 5.20 2 5.26 2 3.6 3.5m: End of Borehole, high suction 22 22 28 5.00 2 3.5m: End of Borehole, high suction 22 22	0.5		\[ALLUVIUM]			×v					
1.0 At 0.6m; Moist. [ALLUVIUM] 99 3.90 0.5 1.0 1m: Becomes stiff with occasional plant fibers. 99 3.95 0.5 1.2m; Moist to wet. 4.00 0.5 4.00 0.5 1.5m; Wet. 1.5m; Wet. 59 4.20 1 1.7m; Becomes grey. 4.30 2 4.30 2 0rganic Sity CLAY, Dark brown, stiff, wet, moderate to highly plastic. 4.40 1 4.30 2 2.0 Clayey SILT. Grey, firm, wet to saturated, moderately plastic. [ALLUVIUM] 28 4.45 1 2.5m: Becomes stiff with poor recovery and some contamination from above. 57 4.95 1 3.0 3m: Fully saturated. 57 4.95 1 3.6 3.5m: End of Borehole, high suction 22 28 5.10 2 3.6 3.5m: End of Borehole, high suction 22 28 5.10 2 3.6 3.5m: End of Borehole, high suction 22 28 5.00 2 3.6 3.5m: End of Borehole, high suction 22 5.30 2 <td></td> <td></td> <td>Silty CLAY. Orange and light grey, very stiff, dry to</td> <td></td> <td></td> <td>× × ×</td> <td></td> <td></td> <td></td> <td></td> <td></td>			Silty CLAY. Orange and light grey, very stiff, dry to			× × ×					
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	-		At 0.6m; Moist. [ALLUVIUM]			* *					
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	10-				sits	× ×		1 I 1 I 1 I	99		
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	-		1m: Becomes stiff with occasional plant fibers.		depo	* *			45		
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	-		1.2m: Moist to wet.	19	he	× ×					0.5
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high				5/20	ece	× ×					
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	1.5		1.5m: Wet	\mathbb{N}_{50}^{46}	(Hol	×					
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	-				Σ	* *			34		
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high				19/01	S	* *					1
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	_				ALL	<u></u>			20		1
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	2.0				UP,	<u></u>					1
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high		-			RO	<u>34</u>					1
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	-				0 A	× * × ×					2
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	2.5-				UNG NG	× × ~ ×			62		1
3.0 3m: Fully saturated. 3m: Fully saturated. 3m: Fully saturated. 4.85 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high	2.5				UR/	<u> </u>			28		1
3.0 3m: Fully saturated. 57 4.90 1 3.6 3m: Fully saturated. 57 4.95 1 3.5 3.5m: End of Borehole, high suction 51 5.15 2 3.5 3.5m: End of Borehole, high suction 24 5.25 2	-		some contamination nom above.		TA	× × × ×					1
3.0 3m: Fully saturated. 3m: Fully saturated. 57 4.95 1 3.5 3.5m: End of Borehole, high suction 3.5m: End of Borehole, high suction 511 5.15 2 3.5 3.5m: End of Borehole, high suction 28 5.20 2 3.5m: End of Borehole, high suction 20 5.25 2 3.5m: End of Borehole, high suction 20 5.30 2						<u></u>					1
3.5 3.5m: End of Borehole, high suction 28 5.00 2 3.5m: End of Borehole, high suction 28 5.10 2 3.5m: End of Borehole, high suction 28 5.20 2 3.5m: End of Borehole, high suction 28 5.20 2	3.0					× × × ×			57		1
3.5 3.5m: End of Borehole, high suction			3m: Fully saturated.			~ ~~~ ~~			28		
3.5 3.5m: End of Borehole, high suction 51 5.15 2 3.5m: End of Borehole, high suction 28 5.20 2 5.25 2 5.30 2						× <u>×</u> ××					
3.5 3.5m: End of Borehole, high suction 28 5.20 2 5.25 2 5.30 2	_					×× <_××_					
5.25 2 5.30 2	3.5	ŀ	3.5m; End of Borehole, high suction			<u> </u>					
5.30 2									28		
	_										2
	-									5.35	2
	4.0										
	_										-
5.55 2											2
	45										
4.5											
5.80 2											
5.0 5.85 2 5.90 2	5.0-										

Water

Soils logged in accordance with 'The guidelines for the classification and description of soil and rock for engineering purposes' December 2005, NZGS

Shear Vane

Corrected as per NZGS Guidelines

SOIL DYNE LTD AUCKLAND

Other Comments

Flat, Field. Hole data is for a set

location only.

M: 027 368 8832



▼ Standing Water Level Vane No.:GEO1596 is 1.414 UTP = Unable To Penetrate \bigtriangledown Water Level At + = Peak Exceeded Time Of Drilling

- = No Result

	HAND AUGER LOG								Job No.: 190		051	
Clie	nt:	KGA Geotechnical Group Ltd						Hole No.:		AH4		
Proj	ect:	272-278 Clevedon-Kawakawa Road, Cleve	don						Date:		18/02	/2019
Loca	ation:	See Site Plan							Logge	ed By:	S	R
Coo	rdinat	es:,		Gro	ound L	evel: -			Sheet	:	1 o	f 1
Depth (m)	RL	Subsurface Conditions	Groundwater	Geological Unit	Graphic Log			(kPa	or detai l s		Penetr	ala ometer / 50mm) Blows
		Topsoil. [TOPSOIL]	0		<u>46 46</u>	50			200	values	(m) 3.90	1
				TOP	ETS ∆ ≝ To			Ì			3.90 3.95	1
_		SILT with minor clay. Orange, very stiff to hard, low plasticity. [WAIPAPA GROUP / COLLUVIUM ?]			<						4.00 4.05	1
			1		× · · ·		1	1		198+	4.05	1
0.5		Clayey SILT. Orange mottled light grey, very stiff to hard, dry, low to moderately plastic. [WAIPAPA	1		X					-	4.15	1
_		GROUP / COLLUVIUM ?]			×		1		1		4.20 4.25	1
_		Silty CLAY. Orange mottled light grey, very stiff, dry to moist, moderate to highly plastic. [WAIPAPA			× ×						4.25	1
1.0-		GROUP / COLLUVIUM ?]			×					170	4.35	1
_		0.9m: Becomes moist and highly plastic.		(s	× ×		-	ł		71	4.40	1
-		1.2m: Moderate to highly plastic.		posit	× ,		į	- i			4.45 4.50	1
		Clayey SILT. Light grey mottled orange, very stiff,	1	lep :	°*_* ×_××			Ì			4.55	1
1.5		moist, moderately plastic. [WAIPAPA GROUP / COLLUVIUM ?]		sene	× × ×			Ì		116 57	4.60	1
-		Silty CLAY. Orange mottled light grey, very stiff,		stoc	. x x x		i I I	Ì		57	4.65 4.70	2
		moist, highly plastic.		(Plei	× _ v		1		1		4.75	1
_		At 1.8m; Moist to wet. [WAIPAPA GROUP / COLLUVIUM ?]		Ψſ	× × ×				1	100	4.80	1
2.0					× *				1	102 45	4.85	1 2
_				ALLI	× × ×		1		1		4.90 4.95	2
_			119	UP /	×				1		5.00	2
_		2.3m: Becomes light grey mottled orange and moist.	02/20	RO	× ×			-		158	5.05	3
2.5		Clayey SILT with minor fine sand. Light grey mottled	18/02/2019 18/02/2019	RANGA GROUP ALLUVIUM (Pleistocene deposits)	<u>× ×</u> × <u>×</u> ×		1			71	5.10 5.15	2 2
_		orange, very stiff, wet, moderately plastic. [WAIPAPA	1 20/61	DNG	<u> </u>						5.20	2
_		SILT with CLASTS (<3mm), some fine sand and					i	į			5.25	2
		minor to trace of clay. Light brown mottled orangey		TAU			1	į	1	156	5.30 5.35	2 3
3.0		brown and light grey, very stiff, wet, low plasticity. At 3m; With Clasts (<5mm), wet to saturated and								28	5.40	2
-		orange and light grey. [WAIPAPA GROUP /	ł		× ×		1	ł			5.45	3
-		COLLUVIUM ?] Fine to medium, loose Sandy SILT with Clasts			x x x x			ł			5.50 5.55	2 3
3.5-		(<5mm) and minor clay. Orange, wet to saturated,	ļ		× × × ×				1	99	5.55 5.60	3 2.5
-		ow plasticity. [WAIPAPA GROUP / COLLUVIUM ?]			× ×			ł	1	42	5.65	2.5
-		Silty CLAY. Orange mottled light grey and dark			× •			1			5.70 5.75	2.5
		orange, stiff, wet, highly plastic. [WAIPAPA GROUP /			×		-			54 31	5.75 5.80	2.5 2.5
4.0		Silty (Fine to coarse, loose) SAND with Clasts									5.85	2.5
-		(<7mm) and minor clay. Light grey mottled orange, wet to saturated, low plasticity. [WAIPAPA GROUP /									5.90	3
		COLLUVIUM ?]						i	1		5.95 6.00	3 3
-		Silty CLAY. Light grey and orange, stiff, wet,					i I I	i I I	i I I		6.05	3
4.5		moderate to highly plastic. [WAIPAPA GROUP / COLLUVIUM ?]									6.10	3
		3.85m: End of Borehole, high suction				1			1		6.15 6.20	3 3
		e, som. End of Borenoie, high subtion					1	ł	1 1 1		6.20	3
-								ł			6.30	3
5.0							1	÷	1			

Water

Time Of Drilling

Soils logged in accordance with 'The guidelines for the classification and description of soil and rock for engineering purposes' December 2005, NZGS

- = No Result

AUCKLAND **Other Comments** Shear Vane ▼ Standing Water Level Near Level, Field. Hole data is Corrected as per NZGS Guidelines M: 027 368 8832 Vane No.:GEO1596 is 1.414 for a set location only. UTP = Unable To Penetrate \square Water Level At + = Peak Exceeded E: soil.dyne@yahoo.com

7 Soil Dyne Ltd

SOIL DYNE LTD

		HAND AUGER	Jo	Job No.: 19005		051						
Clie	nt:	KGA Geotechnical Group Ltd						Но	le No.:	AH5		
Proj	ect:	272-278 Clevedon-Kawakawa Road, Cleve	edon					Dat	e:	14/02	2/2019	
Loca	ation:	See Site Plan						Log	ged By:	S	R	
Coo	rdinat	es: ,		Gro	ound L	evel: -		She	eet:	1 c	1 of 1	
Depth (m)	RL	Subsurface Conditions	Groundwater	Geological Unit	Graphic Log		() refer note	ear Strei (Pa) es for deta	-	Penetr (blows _{Depth}	ala ometer / 50mm) Blows	
		Topsoil. [TOPSOIL]			<u>46 46</u>					(m) 3.60	5	
				TOPSOI L	ETS A					3.65	5 4	
_		Clause SILT Orange mettled light group hard dry	-	Ĕ	<u>6 3613</u> (x x					3.70	4	
_		Clayey SILT. Orange mottled light grey, hard, dry, low to moderately plastic. [WAIPAPA GROUP /			× × ×		1		UTP	3.75 3.80	4 5	
0.5		COLLUVIUM ?]			×××		I I	I I I I	-	3.85	6	
		Silty CLAY. Orange mottled light grey, hard, moist,	1		X V					3.90	4	
_		highly plastic. [WAIPAPA GROUP / COLLUVIUM ?]			× •					3.95	5	
_				6	× ×				141	4.00	3	
1.0		1m: Very stiff.		osits	× ×		1		141 57	4.05	4 3	
-				TAURANGA GROUP ALLUVIUM (Pleistocene deposits)	×					4.10 4.15	3 4	
		1.2m: Moist to wet.		ue c	× ×					4.20	4	
				leoc	× ×					4.25	5	
1.5				eisto	* *				99	4.30	7	
_		1.5m: Stiff.		P <u></u>	×				31	4.35	6	
-		Clayey SILT with minor fine sand. Light grey mottled	1	ΜΩ	× <u>× × ×</u>					4.40	8 9	
-		orange, stiff, moist to wet, moderately plastic.			ČX (X.)		1	1		4.45 4.50	9 4	
					х х х.	i	I	i i	UTP	4.55	4	
2.0		SILT with Clasts (<3mm<25%), some fine sand and minor clay. Orange, light grey and dark orange, stiff,		d d	× × ×		I I		-	4.60	5	
_		moist to wet, low plasticity. At 2m; Hard. At 2.2m;		SoL	x x x					4.65	4	
_		With some clasts (<4mm), [WAIPAPA GROUP /		Б	× * * *					4.70	7	
-		COLLUVIUM ?] 2.4m: With some clay and wet.		IGA	· · · · · · · · · · · · · · · · · · ·	1	I I		UTP	4.75	10	
2.5				AN	к. × × ×		1		-	4.80 4.85	11 11	
_		Fine to medium, medium dense to dense Sandy	6 6	AUF	· × × ×.		I I	i i		4.90	11	
_		SILT with clasts (<4mm) and minor clay. Orange mottled light grey and dark orange, wet, low	/2019 /2019	Η	к. 8 × 8					4.95	14	
_		plasticity. [WAIPAPA GROUP / COLLUVIUM ?]	14/02/2 19/02/2		× × ×		1		UTP	5.00	14	
3.0			ŽŤ		x x x x		1	I I I I	-			
					× × × ×							
_					x x x							
_		Silty (Fine to medium, medium dense to dense) SAND with Clasts (<5mm<30%) and minor to trace			× ×.							
3.5		of clay. Orangey brown, wet, very low plasticity.	ļ		×		i.	i i	UTP			
-		[WAIPAPA GROUP / COLLUVIUM ?]	1									
		3.55m: End of Borehole, unable to penetrate										
_												
4.0							I I					
_												
-												
						1						
4.5-												
-												
-												
50-												

Soils logged in accordance with 'The guidelines for the classification and description of soil and rock for engineering purposes' December 2005, NZGS

Water ▼ Standing Water Level \bigtriangledown Water Level At

Produced with Core-GS

Other Comments Shear Vane Flat, Field. Hole data is for a set Corrected as per NZGS Guidelines M: 027 368 8832 Vane No.:GEO1596 is 1.414 location only. UTP = Unable To Penetrate + = Peak Exceeded E: soil.dyne@yahoo.com Time Of Drilling - = No Result

SOIL DYNE LTD AUCKLAND

Soil Dyne Ltd

	HAND AUGER LOG								190051	
Clier	nt:	KGA Geotechnical Group Ltd					Hole	No.:	Ał	16
Proj	ect:	272-278 Clevedon-Kawakawa Road, Cleve	don				Date:		14/02	/2019
Loca	ation:	See Site Plan					Logge	d By:	SF	२
Coo	rdinate	es:,		Gro	ound L	evel: -	Sheet:		1 of	f1
Depth (m)	RL	Subsurface Conditions	Groundwater	Geological Unit	Graphic Log	Vane Shear (kPa (refer notes fo	n) or details)		Sca Penetro (blows / Depth	ometer
		Topsoil. [TOPSOIL]	0		<u>46 46</u>	50 100 150	200	Values	(m) 2.05	
		Clayey SILT. Grey mottled orange and brown, very stiff, dry, low to moderately plastic. At 0.4m; Becomes moderately plastic, dry to moist and light grey mottled orange. [ALLUVIUM] Silty CLAY. Orange and grey with brown staining, very stiff, moist, highly plastic. [ALLUVIUM]		GROUP ALLUVIUM (Holecene deposits) SOIL	2 TS <u>a</u> 	22		144 31	2.10 2.15 2.20 2.25 2.30 2.35	1 2 2 2 3 3 4
_ _ 1.0— _		0.9m: With some clasts (<3mm), moist to wet with occasional organics (<3mm). At 1m; Extra sensitive.	2/2019	0H) MUIVU	× × ×			113 14	2.40 2.45 2.50 2.55	4 5 6
 1.5		Fine to medium, loose Sandy SILT with Clasts (<5mm), Gravels (<20mm) and some clay. Grey mottled orange and brown, wet, low plasticity. At 1.5m; With GRAVELS (30-40%) and light grey mottled orange. [ALLUVIUM]	19/02/2019	A GROUP ALLI				UTP -	2.60 2.65 2.70 2.75 2.80	7 7 7 7 8
2.0		Medium dense to dense CLASTS (<5mm), GRAVELS (<20mm), Silt, fine to medium Sand and a trace of clay. Light grey and orange, wet to saturated, no plasticity. [ALLUVIUM] Silty CLAY. Bluish grey, hard, moist to wet, highly plastic. [ALLUVIUM]		TAURANGA	****** *******	22228		141 57	2.85 2.90 2.95 3.00 3.05 3.10	9 9 10 10 11 11
 2.5 		2m: End of Borehole, high suction / granular material from above prevents extraction							3.15 3.20	12 11
3.0— — — —										
3.5										
 4.0 										
4.5										
5.0-				1			1			

Soils logged in accordance with 'The guidelines for the classification and description of soil and rock for engineering purposes' December 2005, NZGS

Produced with Core-GS

Water **Other Comments** Shear Vane ▼ Standing Water Level Near Level, Field. Hole data is Corrected as per NZGS Guidelines M: 027 368 8832 Vane No.:GEO1596 is 1.414 for a set location only. UTP = Unable To Penetrate \square Water Level At + = Peak Exceeded E: soil.dyne@yahoo.com Time Of Drilling - = No Result

-Soil Dyne Ltd

SOIL DYNE LTD AUCKLAND

HAND AUGER LOG								Job No.: 190		051
Clie	nt:	KGA Geotechnical Group Ltd					Hole No.:		AH7	
Proj	ect:	272-278 Clevedon-Kawakawa Road, Cleve	edon				Date:		14/02	/2019
Loca	ation:	See Site Plan					Logged	By:	S	२
Coo	rdinate	es: ,		Gro	ound L	evel: -	Sheet:	-	1 0	f 1
Depth (m)	RL	Subsurface Conditions	Groundwater	Geological Unit	Graphic Log	Vane Shear (kPa (refer notes fo	ı) – – – – – – – – – – – – – – – – – – –	ı	•	
			อั		-	50 100 150	200	Values	Depth (m)	Blows
_		Topsoil. [TOPSOIL]		SOIL	≥_L2_7				2.65	5
		SILT with some clay. Orange mottled brown, very stiff to hard, dry, low plasticity. [WAIPAPA GROUP / COLLUVIUM ?] Clayey SILT. Orange mottled light grey, very stiff to hard, dry, low to moderately plastic. [WAIPAPA GROUP / COLLUVIUM ?] 0.7m: Moderately plastic. 0.9m: Becomes moist. 1m: Becomes hard. SILT with some clay, some clasts (<3mm) and some fine sand. Orange mottled light grey, hard, moist, low plasticity. At 1.3m; With minor clay. At 1.5m; With Clasts (<4mm<25%), minor to trace of clay and orange mottled brown, black, light grey and dark orange. [WAIPAPA GROUP / COLLUVIUM ?] Fine to medium, medium dense Sandy SILT with Clasts (<3mm) and minor to trace of clay. Dark orange mottled orange, moist to wet, very low plasticity. At 1.9m; Wet. [WAIPAPA GROUP / COLLUVIUM ?] Silty (Fine to medium, medium dense to dense) SAND with Clasts (<4mm) and a trace of clay. Light brown, orangey brown, orange and dark orange, wet, no plasticity. At 2.4m; With Clasts (<5mm). [WAIPAPA GROUP / COLLUVIUM ?] SILT with some fine sand, some clasts (<5mm) and a trace of clay. Orangey brown mottled orange and brown, hard, moist to wet, no plasticity. [WAIPAPA GROUP / COLLUVIUM ?] 2.6m: End of Borehole, unable to penetrate	14/02/2019	TAURANGA GROUP ALLUVIUM (Pleistocene deposits) SOIL				198+ - UTP - UTP - UTP -	2.65 2.70 2.75 2.80 2.95 3.00 3.05 3.10 3.15 3.20 3.25 3.30 3.35 3.40 3.45 3.50 3.55 3.60 3.65 3.70 3.75 3.80 3.95 4.00 4.05 4.10 4.15 4.20 4.25 4.30 4.55 4.60	5644445645442234667878784467674445567867
5.0-										

Soils logged in accordance with 'The guidelines for the classification and description of soil and rock for engineering purposes' December 2005, NZGS

Water ▼ Standing Water Level

Produced with Core-GS

AUCKLAND **Other Comments** Shear Vane Corrected as per NZGS Guidelines Flat, Field. Hole data is for a set M: 027 368 8832 Vane No.:GEO1596 is 1.414 location only. UTP = Unable To Penetrate \square Water Level At + = Peak Exceeded E: soil.dyne@yahoo.com Time Of Drilling - = No Result

Soil Dyne Ltd

SOIL DYNE LTD

	HAND AUGER LOG									Job No.:		051
Clie	nt:	KGA Geotechnical Group Ltd		Hole	No.:	Α	H8					
Proj	ect:	272-278 Clevedon-Kawakawa Road, Cleve	2-278 Clevedon-Kawakawa Road, Clevedon								14/02	2/2019
Loca	ation:	See Site Plan							Logg	ed By:	S	R
	rdinate	es: ,		Gro	ound L	evel:	_		Shee		1 c	of 1
		· ·	۲.						_		6.	-1-
Depth (m)	RL	Subsurface Conditions	Groundwater	Geological Unit	Graphic Log			(kPa	Streng a) or details		Penetr (blows	ala ometer / 50mm)
			ອັ		-	50	100	150	200	Values	Depth (m)	Blows
_		Topsoil. [TOPSOIL]		TOP	≥ TS ⊴ ≥ TS ⊴						5.05 5.10	1
		SILT some clay. Orange mottled grey, very stiff, dry,	1								5.15	0.5
_		low plasticity. [ALLUVIUM]	-		× × ×			i i		470	5.20	0.5
0.5		Clayey SILT. Light grey mottled orange, very stiff, \dry to moist, moderately plastic. [ALLUVIUM] //			××					170	5.25	0.5
_		Silty CLAY. Orange mottled light grey and dark			×					42	5.30	0.5
_		orange, very stiff, moist, highly plastic. At 0.8m;			×		i.				5.35	1
_		Becomes grey mottled orange. At 0.9m; With a trace			× ×						5.40	2
_		of fine sand and moist to wet.			×		-			0.0	5.45	2
1.0		At 1m; Becomes stiff and light grey mottled orange.			×	777				82	5.50	2
-		[ALLUVIUM]			× ×				i i	40	5.55	1
_		SILT with loose CLASTS (<4mm) and some fine	19						1		5.60	2
-		sand and minor clay. Light grey mottled orange, wet,	14/02/2019		× × 0.						5.65	2
_		low plasticity. [ALLUVIUM]	4/0		******		i i			105	5.70	2
1.5		Silty CLAY with minor clasts (<3mm). Orange and	-	ts)	×		-		i i	105	5.75	3
-		light grey, very stiff, moist to wet, highly plastic.		osi	8					17	5.80	4
-		At 1.8m; With some clasts (<4mm) and orange		lep	×						5.85	4
_		mottled light grey and dark grey plus wet.		e d	× ×		i i	i i			5.85	4 5
_				Ğ	×		1		1	50		
2.0		At 2m; Stiff. [ALLUVIUM]		GROUP ALLUVIUM (Holecene deposits)	×		-		1	59	5.95	8
-				Ĕ	× ×					25	6.00	9
_		Clayey SILT. Orange mottled light grey, stiff, wet,	1	Σ	<u></u>		i i	i.	i i		6.05	8
_		moderately plastic. [ALLUVIUM]	6	l €	× × ×				1		6.10	7
-			₩ S	5	× × ×					99	6.15	4
2.5		Silty CLAY. Light grey mottled orange, stiff, wet,	9/02/2019	ALI	x x	77 -			i i	28	6.20	4
_		highly plastic. [ALLUVIUM]	19/	<u>d</u>	×				1	20	6.25	7
_				Ы	×						6.30	8
				E C C	× ~		i i		1		6.35	10
				∢	×				1	59	6.40	10
3.0-		Clayey SILT. Light grey and orange, stiff, saturated,	1	Ž	<u>× ×</u>					20	6.45	8
		moderately plastic. Poor recovery. [ALLUVIUM]		A A	× × ×					20	6.50	9
				TAURANG	× * × ×		i i		I I		6.55	10
				Ĥ	<u> </u>		-		1		6.60	10
3.5-					××				1	34	6.65	9
^{3.3} _		3.5m: Very poor recovery, difficult Id, firm and			* * *		i.	i	1	14	6.70	10
		pushing down.			<u>~~~</u> ~~				1		6.75	9
					<u>× × ×</u>				1		6.80	5
_					×		i i		1		6.85	5
4.0-					<u> </u>		1		1	34	6.90	8
					× × ×					20		
_					****		i i					
					<u> </u>		i.	i	1			
					× × ×				1			
4.5		4.4m: No recovery with no Id.			** ***				1	45		
					× × ×				1	28		
					× × ×			1	1			
									1			
-					×_×××				1	40		
5.0-		Em: End of Porcholo	-				Ì	i.	1	42		
-		5m: End of Borehole							1	11		
-												

Soils logged in accordance with 'The guidelines for the classification and description of soil and rock for engineering purposes' December 2005, NZGS

SOIL DYNE LTD AUCKLAND **Other Comments** Water Shear Vane ▼ Standing Water Level Near Level, Field. Hole data is Corrected as per NZGS Guidelines M: 027 368 8832 Vane No.:GEO1596 is 1.414 for a set location only. UTP = Unable To Penetrate \bigtriangledown Water Level At SOIL DYNE + = Peak Exceeded E: soil.dyne@yahoo.com LTD Time Of Drilling - = No Result

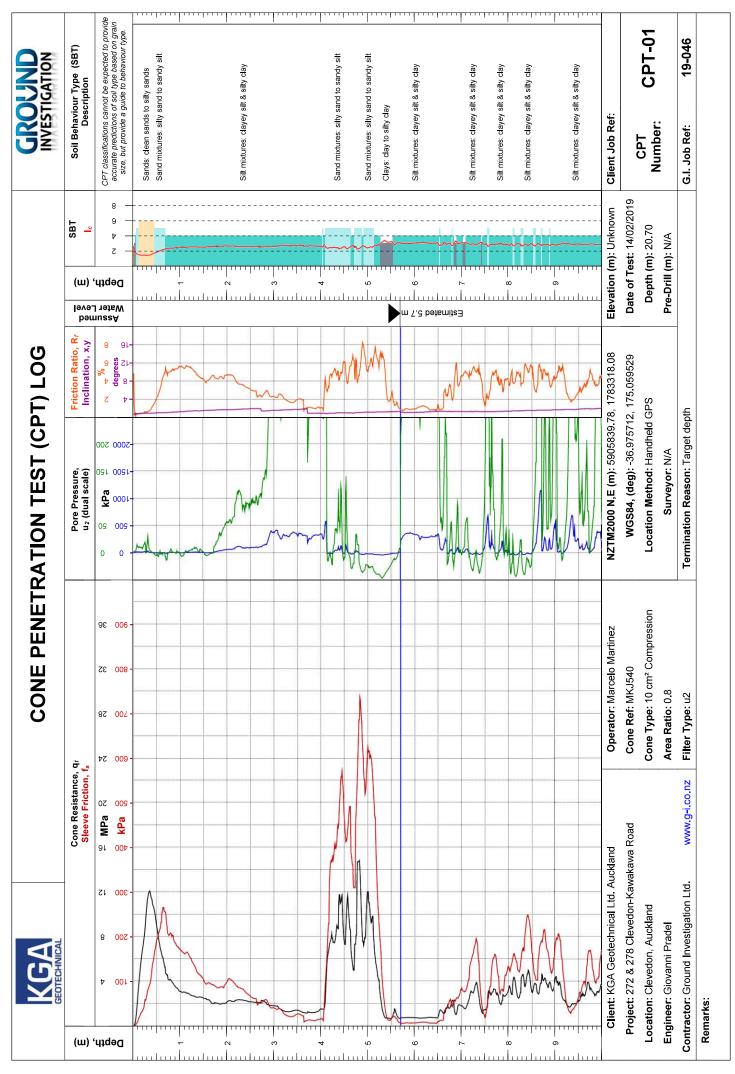
Produced with Core-GS

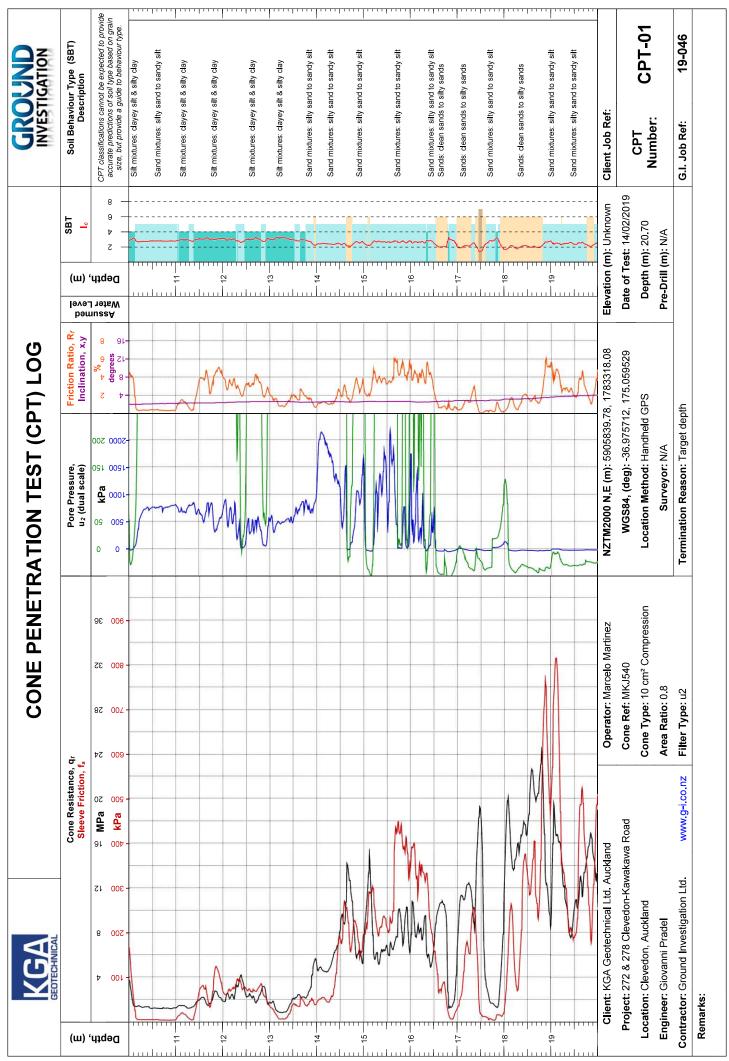




CONE PENETRATION TEST (CPT) LOGS

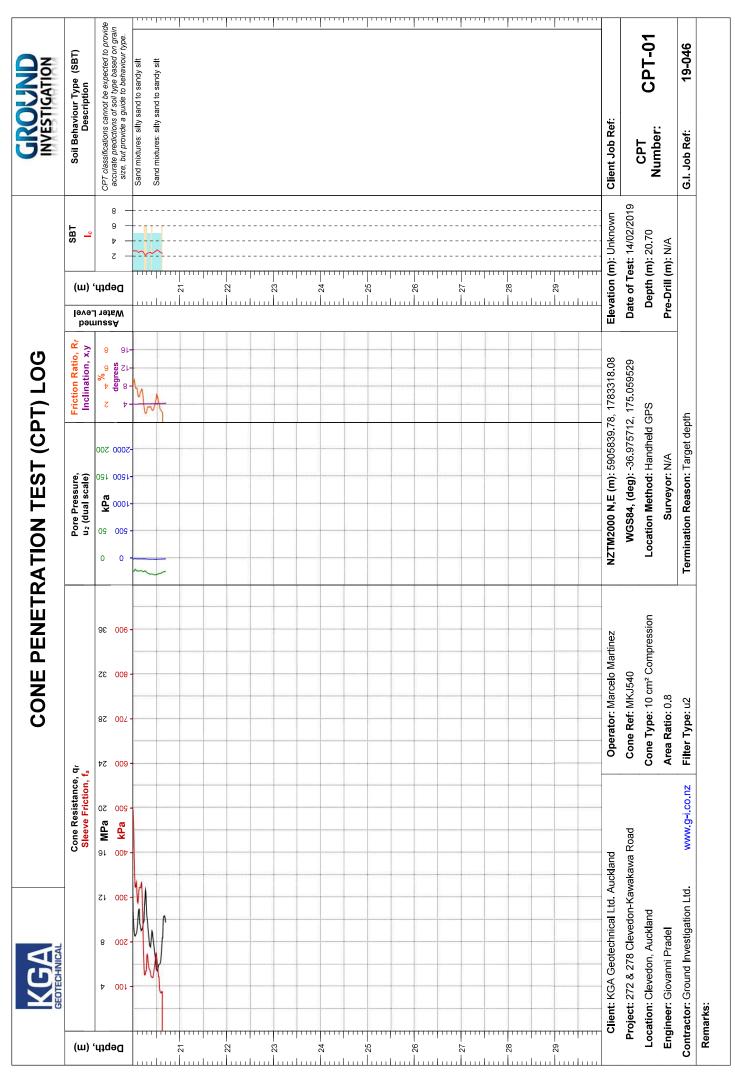


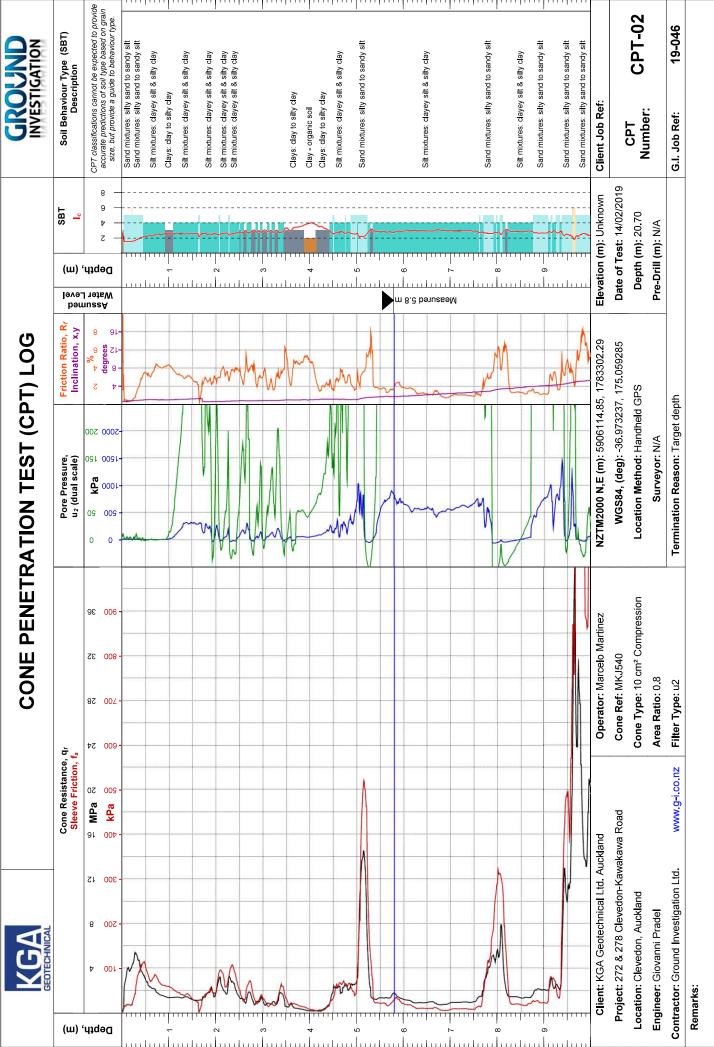




Report Created: 15/02/2019 9:50:43 AM, Page 2 of 3

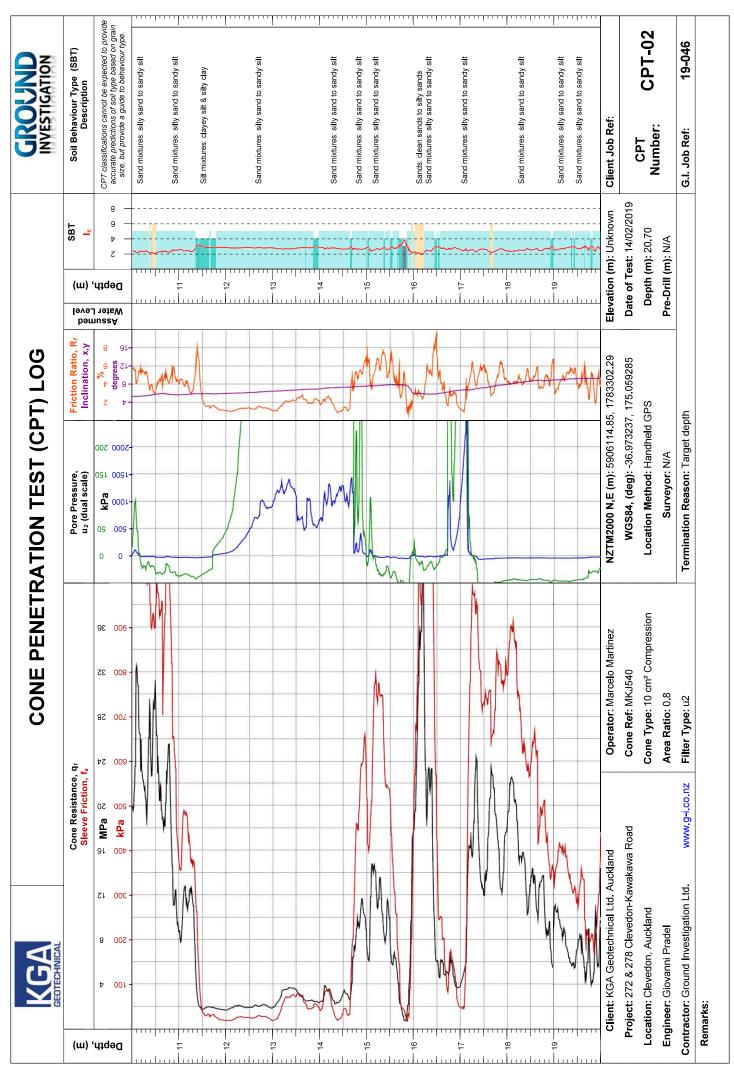


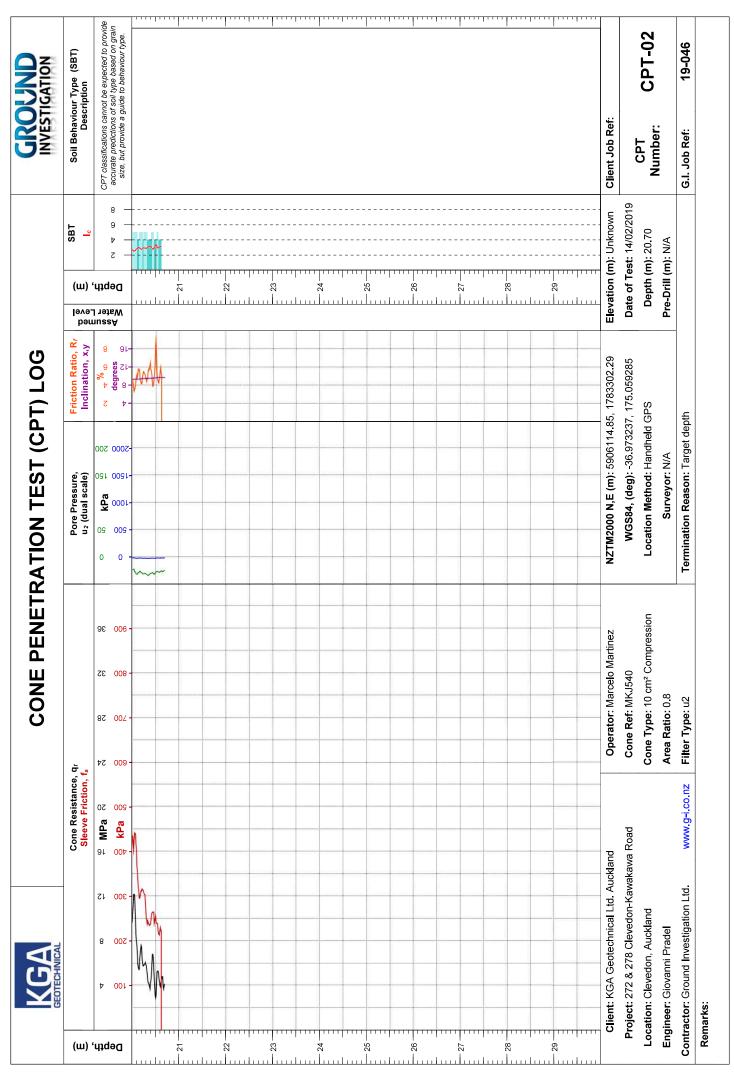




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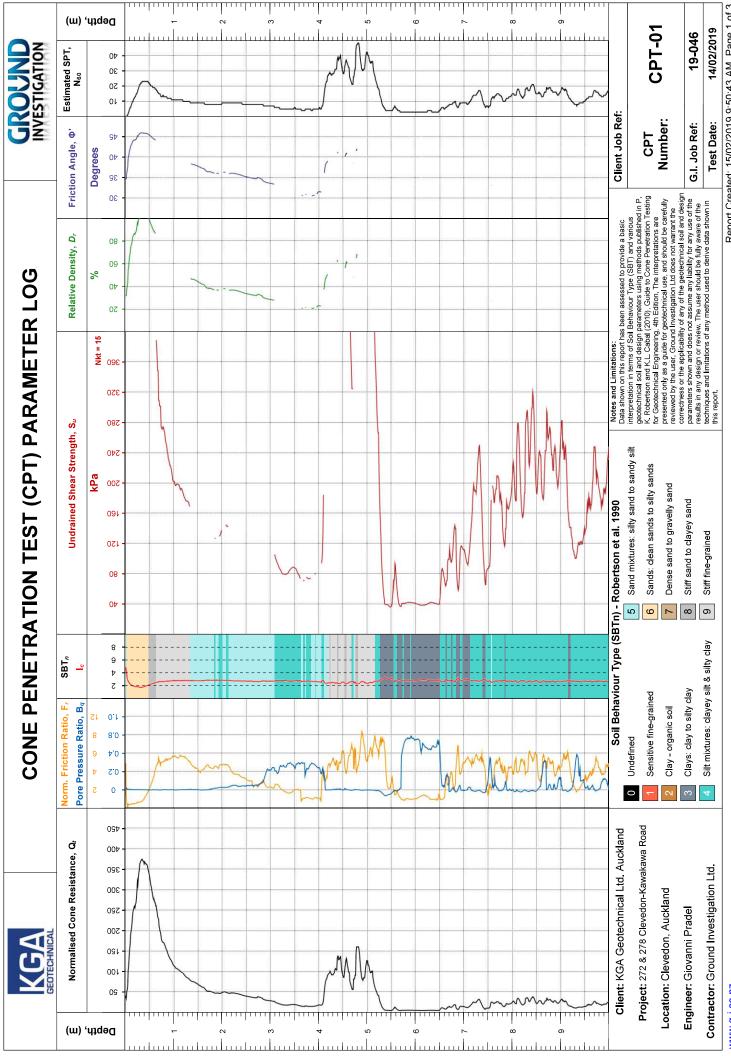




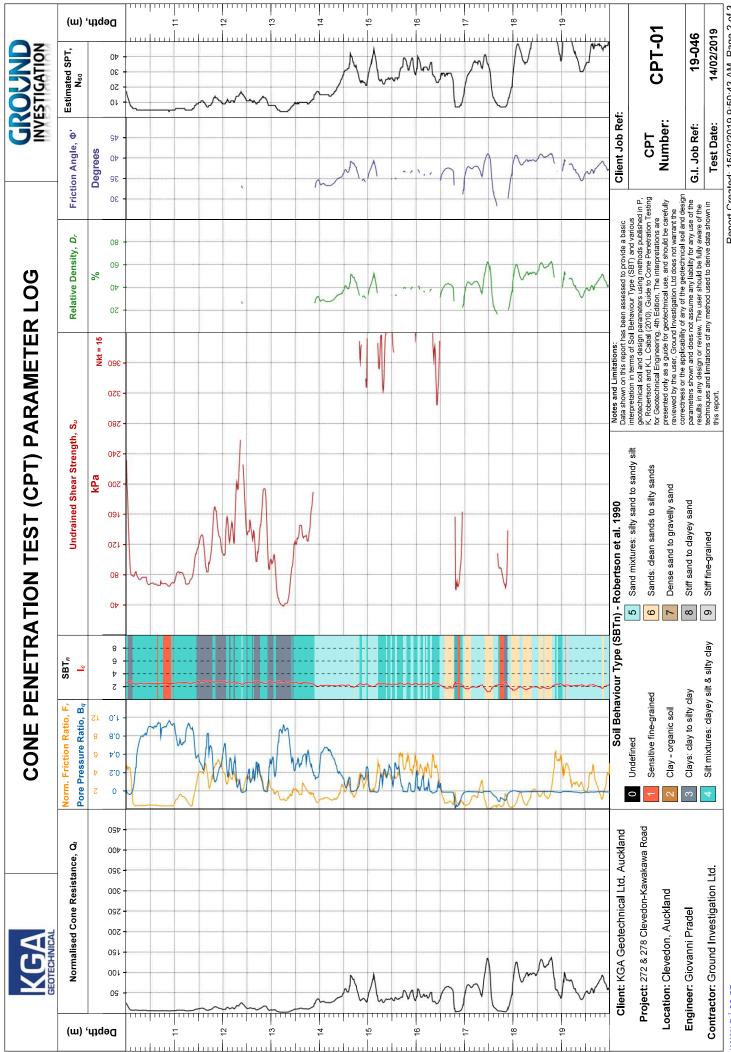




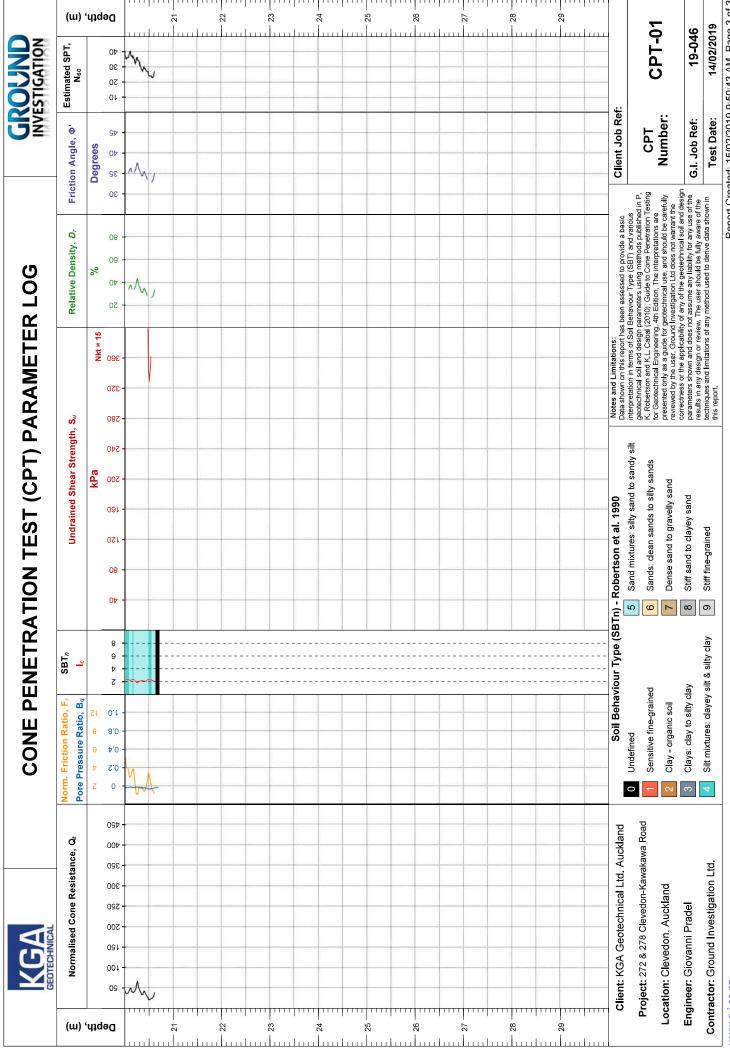
CONE PENETRATION TEST (CPT) PARAMETER LOGS



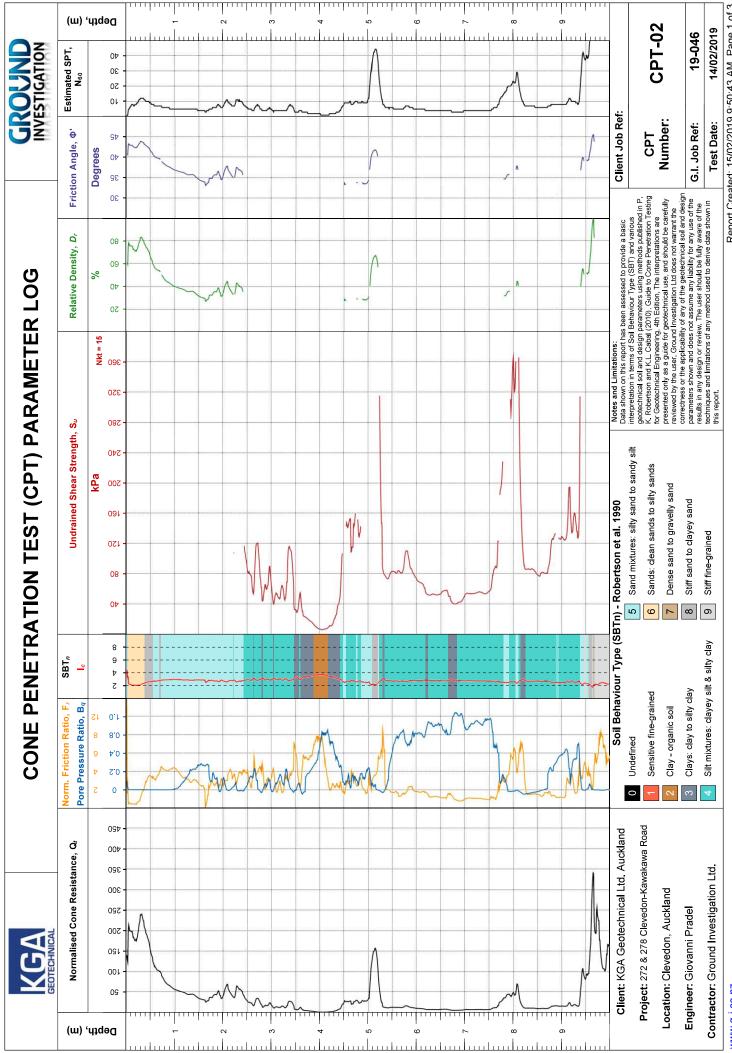
Report Created: 15/02/2019 9:50:43 AM, Page 1 of 3



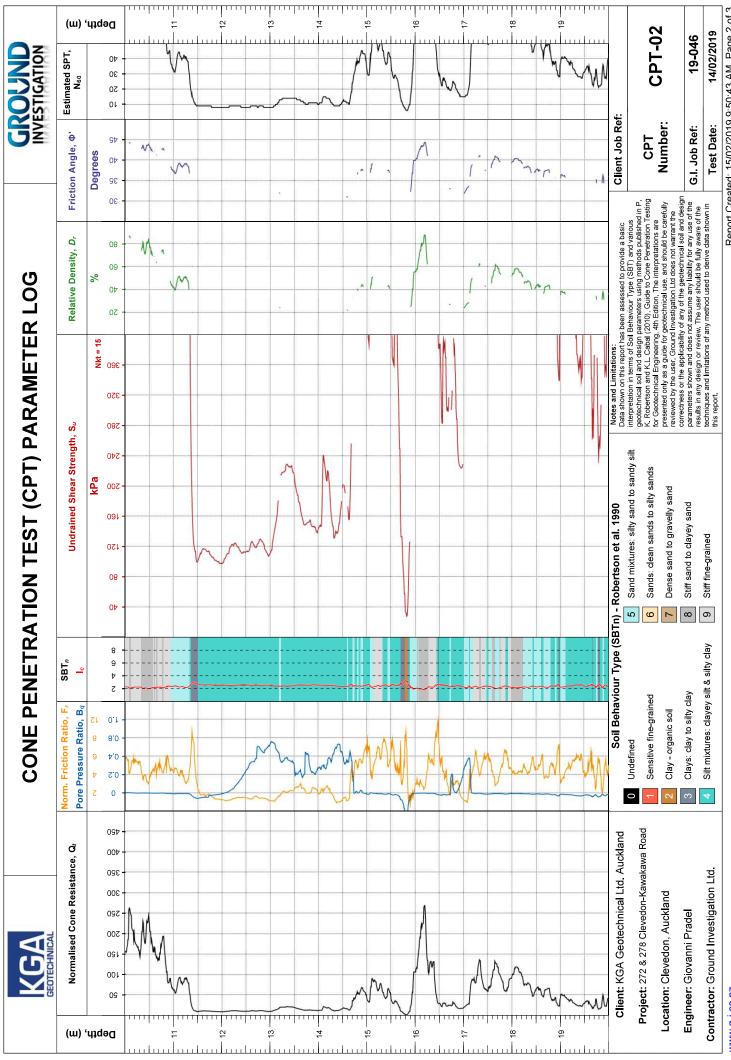
Report Created: 15/02/2019 9:50:43 AM, Page 2 of 3



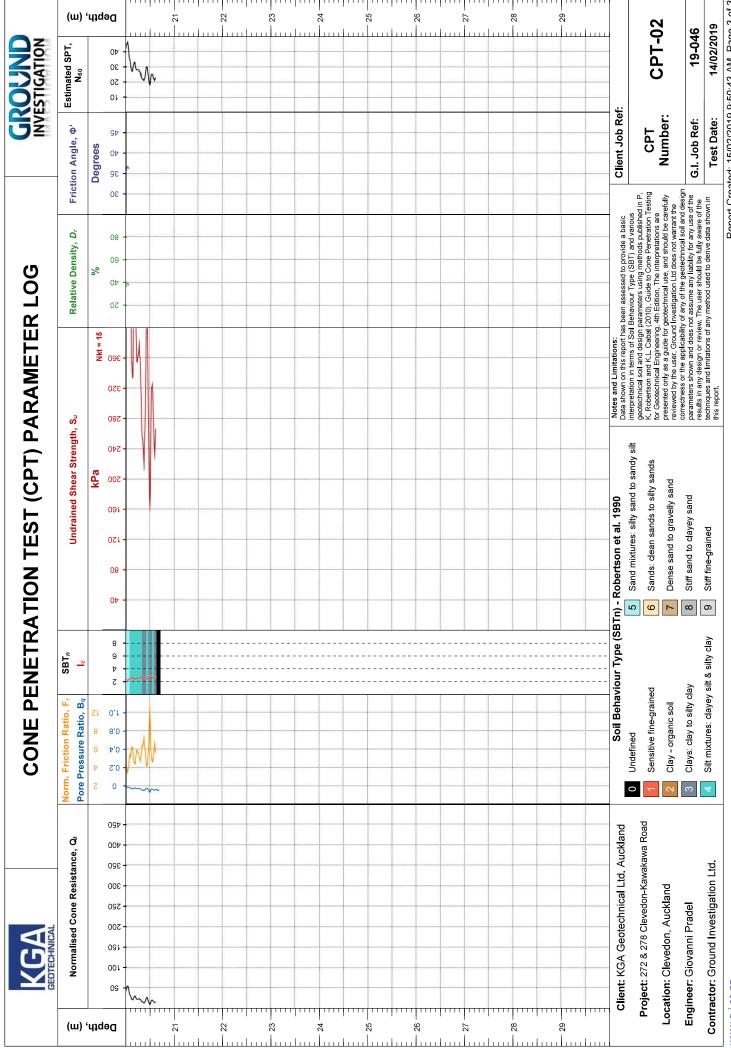
Report Created: 15/02/2019 9:50:43 AM, Page 3 of 3



Report Created: 15/02/2019 9:50:43 AM, Page 1 of 3



Report Created: 15/02/2019 9:50:43 AM, Page 2 of 3



Report Created: 15/02/2019 9:50:43 AM, Page 3 of 3





CPT ZEROS AND DRIFT RESULTS

CPT ZEROS AND DRIFT

272 & 278 Clevedon-Kawakawa Road



G.I. Ref: 19-046

		do: 0		Tip Resistance			Local Friction			Pore Pressure	
Cone Reference	CPT Name	Number	Initial (MPa)	Final (MPa)	Difference (%)	Initial (MPa)	Final (MPa)	Difference (%)	Initial (MPa)	Final (MPa)	Difference (%)
MKJ540	CPT-02	۲	10.612	10.591	0.04	0.129	0.128	0.06	1.444	1.432	0.48
MKJ540	CPT-01	۲-	10.643	10.596	0.09	0.127	0.127	-0.01	1.441	1.440	0.04

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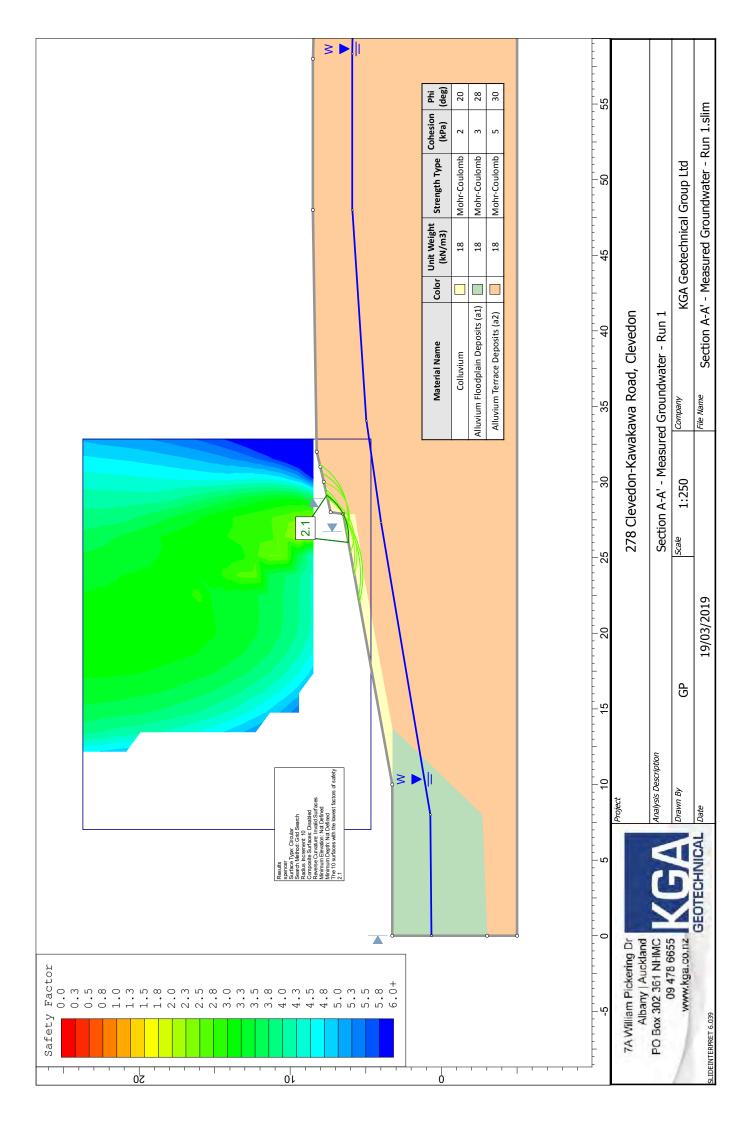
Report Created: 15/02/2019 9:50:43 AM, Page 1 of 1

NOTE: Percentage Zero Difference calculated following ASTM D5778-12. Green indicates a difference between -1% and 1%; yellow shows either -1% to -2% or 1% to 2%; red shows below -2% or over 2%

Project: 272 & 278 Clevedon-Kawakawa Road Client: KGA Geotechnical Ltd. Auckland

Location: Clevedon, Auckland

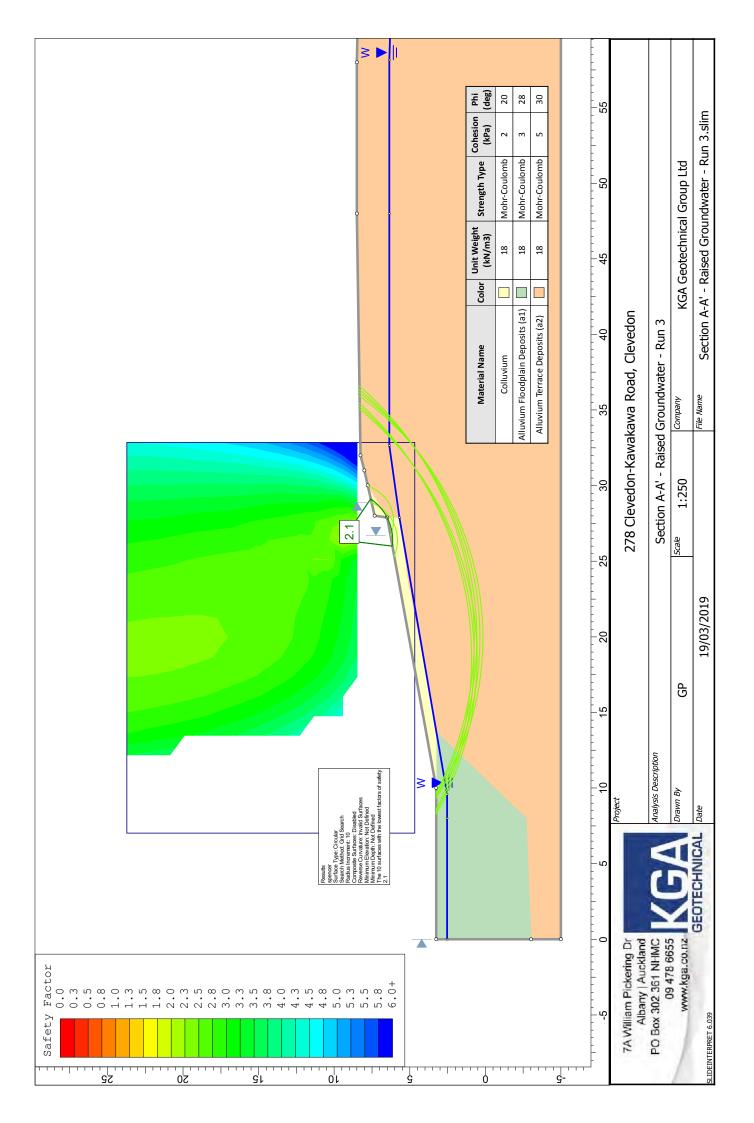
Engineer: Giovanni Pradel

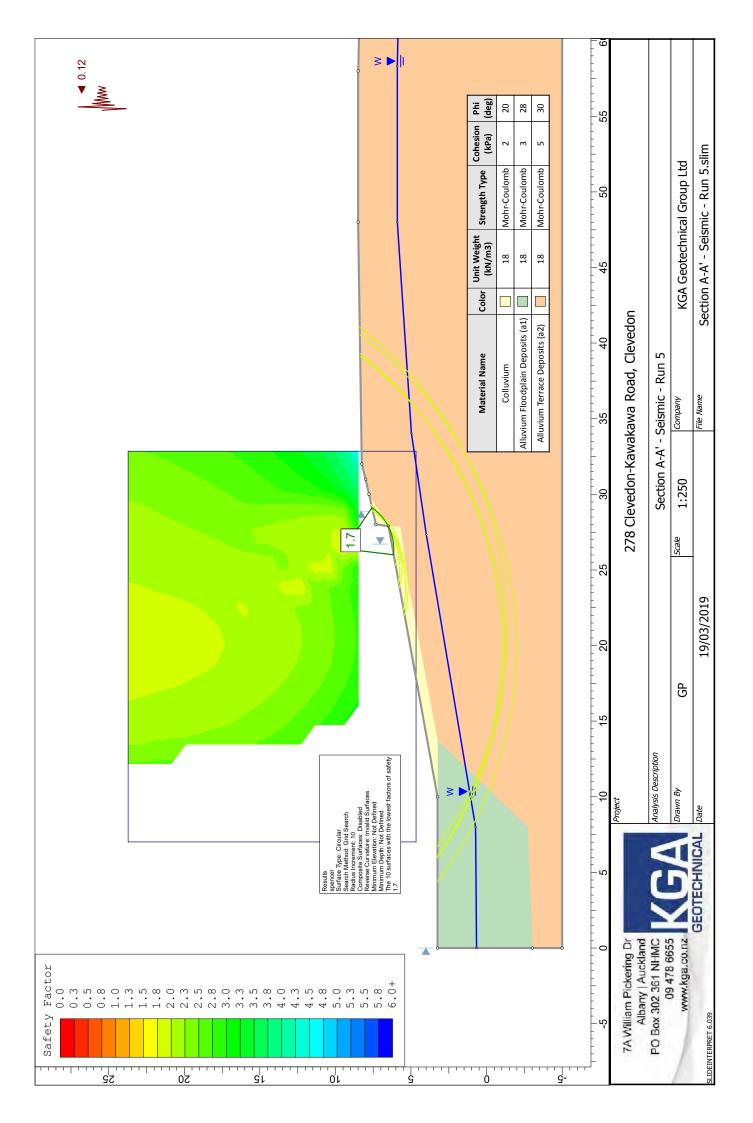




APPENDIX C

Slope Stability Analysis







APPENDIX D

Liquefaction Assessment Results

KGA Geotechnical Group Ltd

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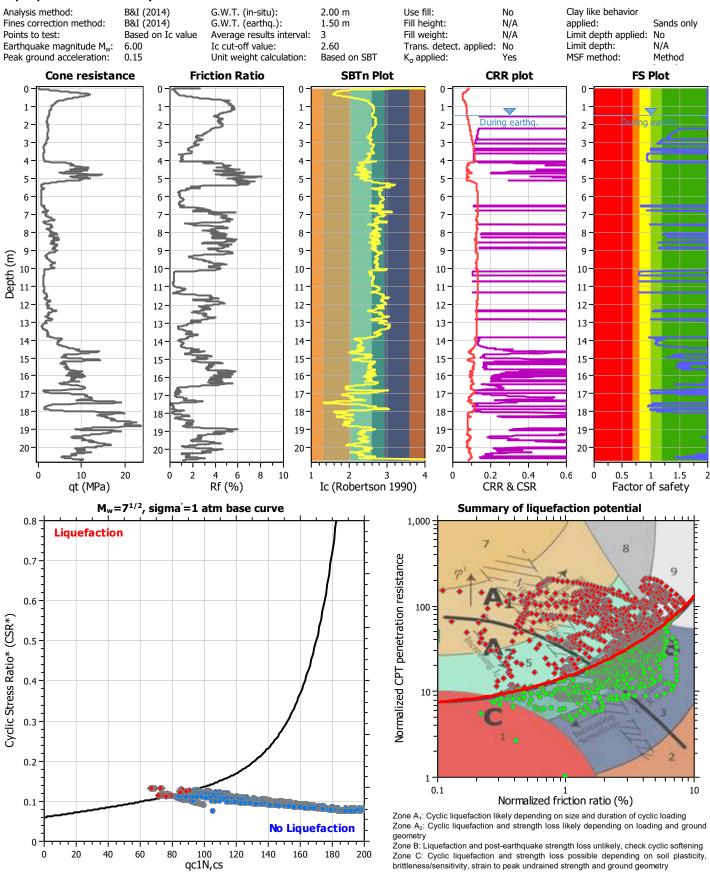
7A William Pickering Drive, Albany PO Box 302 361, North Harbour, Auckland www.kga.co.nz

LIQUEFACTION ANALYSIS REPORT

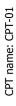
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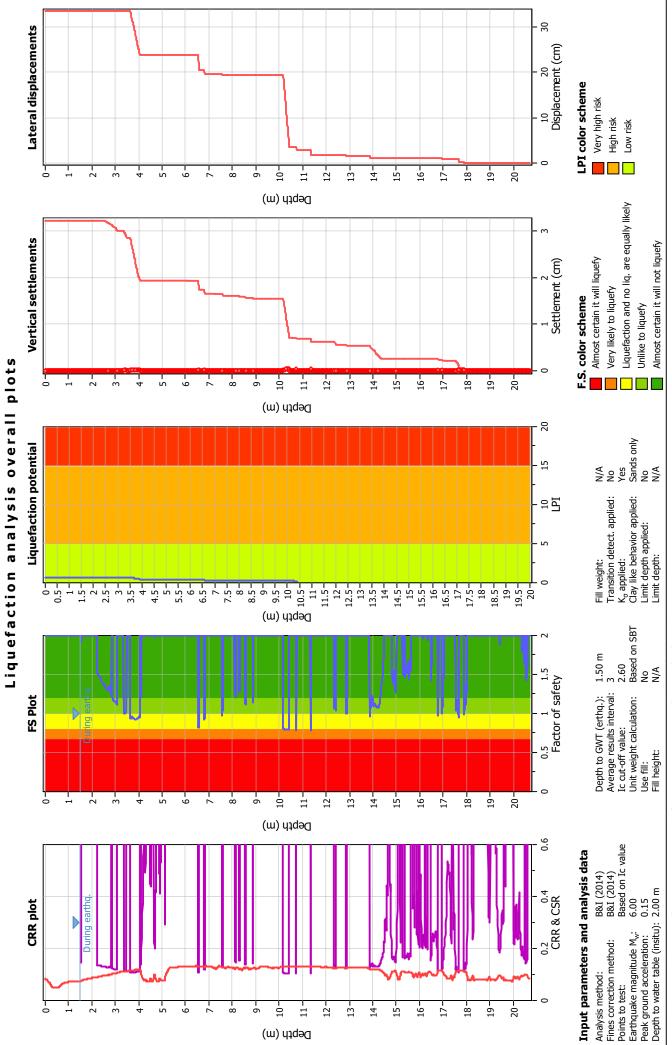
Project title : CPT file : CPT-01

Input parameters and analysis data



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Project file: S-\JOBS ACTIVE\K190000-\K190051 - 272 & 278 Clevedon-Kawakawa Road, Clevedon GP\Logs and Dwgs\Liquefaction Analysis.clq CLiq v.2.3.1.15 - CPT Liquefaction Assessment Software - Report created on: 19/03/2019, 3:30:23 PM

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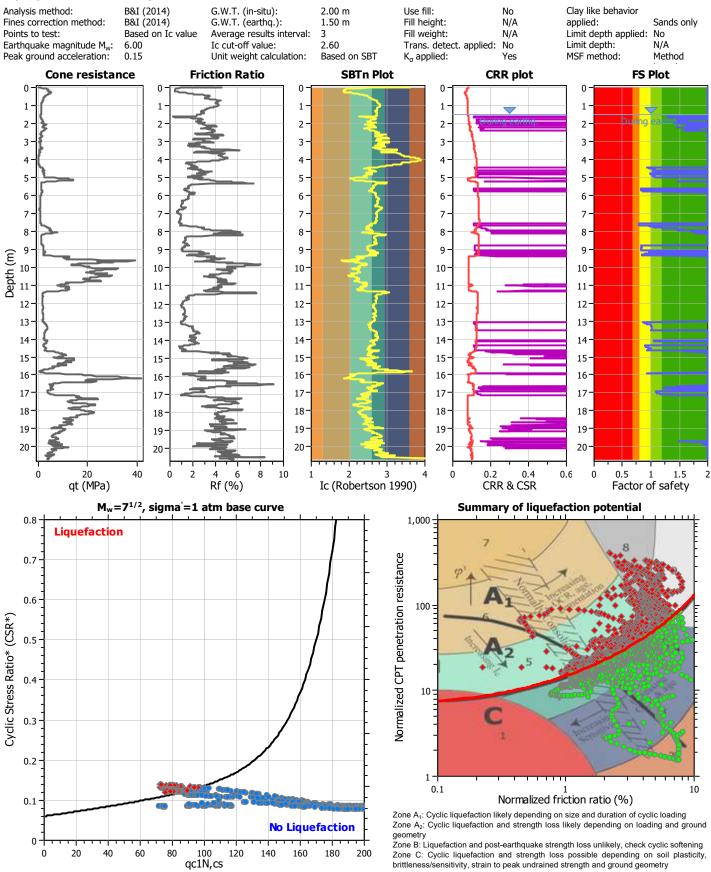
7A William Pickering Drive, Albany PO Box 302 361, North Harbour, Auckland www.kga.co.nz

LIQUEFACTION ANALYSIS REPORT

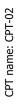
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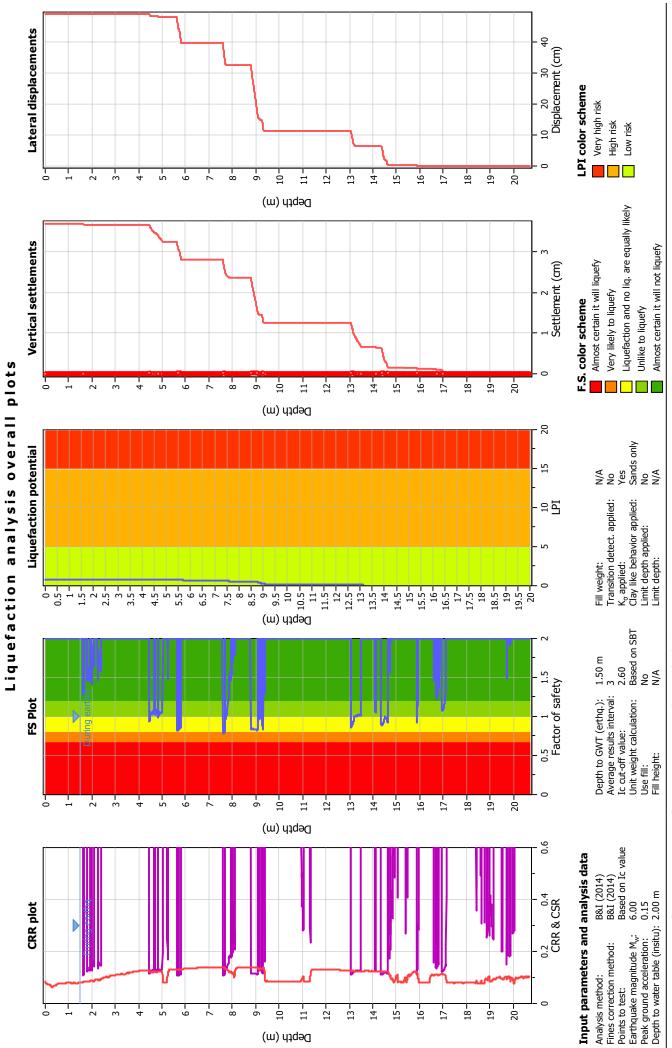
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Input parameters and analysis data



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